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**FOUR COMPUTER CODES FOR DYNAMIC
PROCESS INVENTORY DETERMINATION
APPLICATION IN SAFEGUARDS**

by

A. ROTA

1972



Joint Nuclear Research Centre
Ispra Establishment - Italy

Scientific Data Processing Centre - CETIS

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September 1972

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Luxembourg, September 1972 - 104 Pages - B.Fr. 150.—

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- GROUP — For the optimization of the grouping of fuel elements to be reprocessed.
- CC2 — For the computation of the contribution to the physical inventory of the "two component" mixture.
- CC3 — For the computation of the contribution to the physical inventory of the "three component" mixture.
- MUF — For the final evaluation of the Material Unaccounted. For and its error limits, within a prescribed confidence level.

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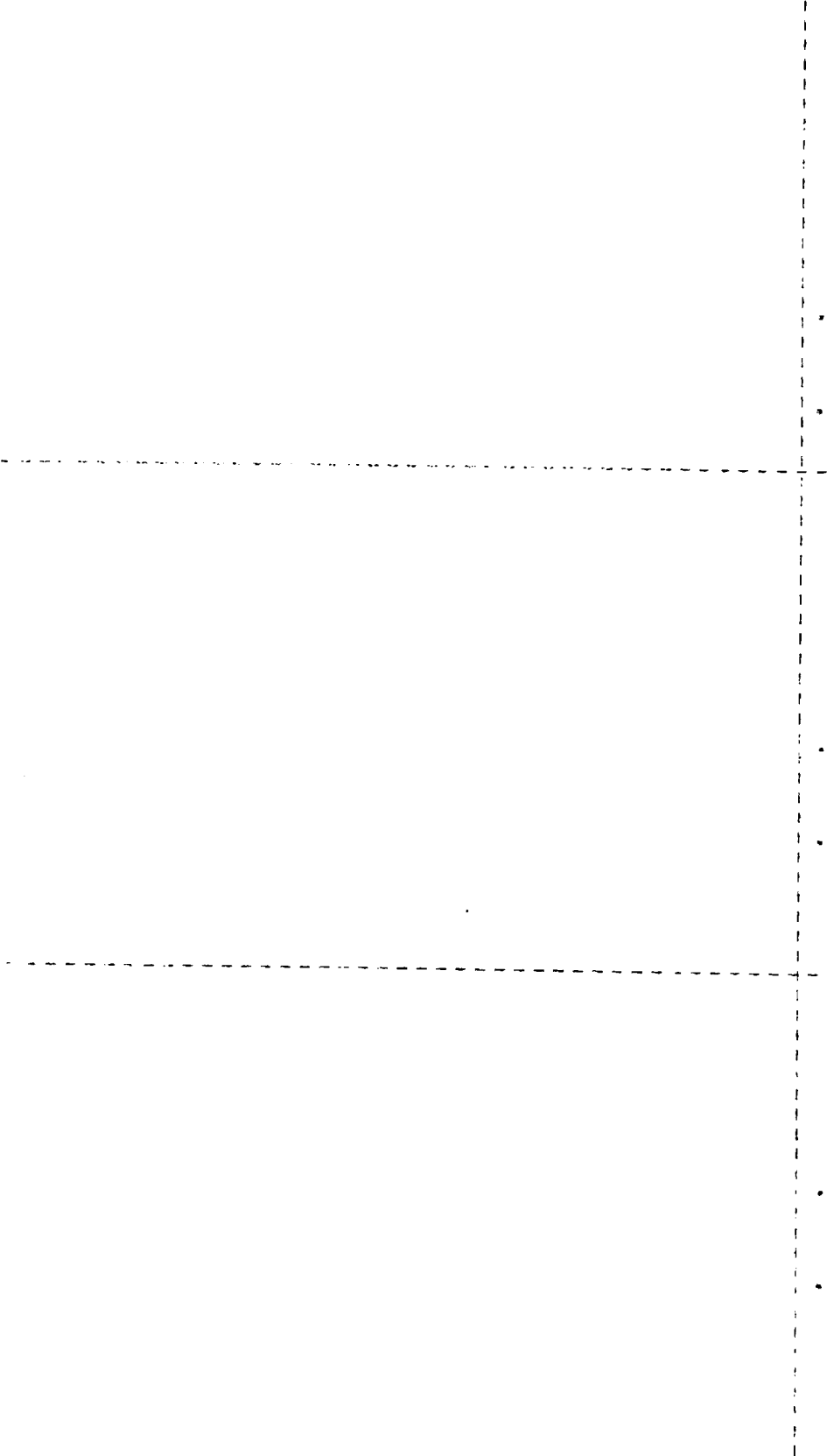
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ABSTRACT

The following computer codes are described and listed. For each of them a sample program is solved.

- GROUP - For the optimization of the grouping of fuel elements to be reprocessed.
- CC2 - For the computation of the contribution to the physical inventory of the "two component" mixture.
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- MUF - For the final evaluation of the Material Unaccounted. For and its error limits, within a prescribed confidence level.

KEYWORDS

PROGRAMMING
INVENTORIES
SAFEGUARDS
MIXTURES

RELIABILITY
FUEL ELEMENTS
REPROCESSING

1. INTRODUCTORY REMARKS

The measurement of the physical inventory of Pu or/and U in a processing plant may be effectuated, during the running of the process, by the DPID technique (Dynamic Process Inventory Determination) [1].

This report is only intended to present four computer codes, that have been written with the purpose of facilitating the implementation of the technique and the handling, in a proper way, of the experimental results. If the reader is interested either to the DPID theory or to the physical background of the codes themselves, he is kindly requested to consult the literature [2].

Copies of the codes, written in FORTRAN language, may be obtained on request from the CETIS Application Program Library.

The reader is supposed to be familiar with the terminology (e.g. batch, superbatches, step, tracer, etc.) inherent to the DPID technique. For this reason the meaning of these particular terms is not defined here and implicit reference is made to the literature [2].

2. THE CODE 'GROUP'

2.1. Outline

This code is designed to help the experimenter in the planning of the input dissolutions of the reprocessing plant, for a correct DPID. In fact, on the basis of the knowledge of the reactor calculation data, concerning the residual Pu and U isotopes present in the fuel elements, the code gives a series of tables, which serve as a guide to the best way of grouping the fuel elements in "dissolution batches". All the available isotopes are sequentially, selected as "tracer". The code may be utilized in two different ways, either to select, from the available material, two groups of dissolution batches (superbatches) with maximum difference of tracer concentration, or to select one group of dissolution batches with minimum variability of tracer concentration. The first solution is chosen when the isotope concentration step for the DPID occurs during the process of the material of one reactor, the second when the step is generated between the materials of two reactors.

2.2. Input data list

- a - The first group of cards (format 20 A4) is a block of 8 FOR-MATS; they must be written as follows: the underlined white spaces must contain the total number of isotopes considered (minimum 02, maximum 10)
- ```
(1H ,16X,'REACTOR DATA', ////,—(2X,2A4), ' FUEL EL. IDENT.'//)
(—F10.3,I4,4A4)
(8X,'FUEL ELEMENT IDENT.',—(2A4,1X),//)
(' ',I10,4A4,—6F9.5)
(/,' BATCH',I3,18X,—F9.5,//)
(1H ,///,' SUPERBATCH MEAN VALUES ',—F9.5)
(13X,'STAND. DEV. ',—F9.5)
(' ',I10,4A4,—F9.5,' PU/U RATIO PERCENT='F7.5)
```



b - One card, format 5I10 with

NELEM = total number of fuel elements

NB1 = number of batches of first superbatches

NB2 = number of batches of second superbatches

MM = number of fuel elements per batch.

Note: if NB1 = 0 only one superbatches is determined with the higher homogenized tracer concentration. If NB2 = 0 only one superbatches is determined with the lower homogenized tracer concentration.

c - One card, format 5I10 with

ISU = number of U-isotopes considered (at least one)

ISP = number of Pu-isotopes considered (at least one)

Note:  $ISU + ISP \leq 10$

: when no Pu or U isotopes are available dummy figures must be introduced.

d - One card; format 5F10.0 with

FACTOR = ratio between the units in which the Pu and U isotopes are given (see group f).

Note: this value is important only for the determination of the Pu/U ratio.

e - One card; with the list of the names of the ISU + ISP considered. For each isotope a field of 8 alphanumeric characters is available. The U isotopes must precede the Pu ones. The maximum number of isotopes is 10.

f - Block of NELEM cards, format 10F6.0, I4, 4A4. The fields I4 and 4A4 are available for proper number and name of the considered assembly a fuel element. The U-isotope quantities (expressed in any unit) present in the fuel element must be punched in the first ISU fields; the sequence must be referred to the one reported in card 'e'. In the following ISP field the analogous information for the Pu isotopes must be given.

### 2.3. Output description

The output of the code GROUP consists of the following set of results:

- Tables with the relevant input data
- A table with the list of the fuel elements available.  
For every element the isotopic content is expressed as relative abundance. Also the  $(\text{Total Pu})/(\text{Total U})$  is provided.
- For every considered isotope (tracer), both of U and Pu, the following data are printed
  - . The list of the elements ordered according to increasing concentration of the selected isotope.
  - . The list (if any) of the elements not considered for the superbatch construction.
  - . The list of the groups of elements of each batch of the first superbatch (minimum homogenized tracer concentration). The mean values of the isotope concentrations for each single batch and for the whole superbatch is given.
  - . Same as before for superbatch two (maximum homogenized tracer concentration).

### 2.4. Remarks

The program has the following limitation: it has been designed for fuel elements having approximately the same U or Pu content, original enrichment and burn-up. The mean values calculated here are, for this reason, not verified. The algorithm used in the program does not ensure that the minimum of the variability or maximum of the difference in tracer concentration is actually achieved. The result is however very close to the optimum one. A more sophisticated program does not seem to be very necessary because of the uncertainty in the calculated reactor data, here used as inputs.

The program is written in double precision for the floating point variables.



### 3. THE CODE 'CC2'

#### 3.1. Outline

The code CC2 evaluates the "two component mixture" contribution,  $H_2$ , to the process inventory.  $H_2$  is given by:

$$H_2 = \sum_{J=1}^{NBATCH} M(J) \frac{X(J) - C2}{C1 - C2} \quad (1)$$

where NBATCH is the number of the output batches,  $M(J)$  is the mass of fissile material (Pu or U) in the  $J$ -th output batch,  $X(J)$  is the relative abundance of the tracer in the same batch,  $C1$  and  $C2$  are the mean tracer concentrations in the two input super-batches.

The code supplies also a statistical interpretation of the parameter  $H_2$ . The uncertainty of  $H_2$  is in fact connected to the experimental unaccuracy of the measured data and to the accepted estimate of  $C1$  and  $C2$ . This error analysis is performed by a Monte Carlo procedure and the result is given as probability density function (pdf) of the dependent random variable  $H_2$ . Error limits around  $\bar{H}_2$  are also estimated for preselected confidence levels.

#### 3.2. Input data list

a - One card as follows:

## INPUT BATCH DATA ##

== The sequence b- to f- must be repeated two times, for the first and the second superbatches respectively ( $K=1,2$ )

b - One card, format 20A4, with the name of the superbatches (e.g. REACTOR CANDU)

c - One card as follows:

BATCH TOTAL — (—) ——— PERC WEIGHT FACTOR

In the first underlined field the element name (PU or U) must be written; in the second the mass unit in the third the tracer name (e.g. Pu-241).

d - One card, format I10, containing NB(K), the number of batches of the K-th superbatches.

e - NB(K) cards, format 2F10.0; every card represents one batch and contains, in sequence, the following data:

- . the total mass of the fissile element contained in the batch
- . the total mass of the tracer in the batch

f - One card as follows:

REACTOR BATCH NUMB.    MEAN PERC.T CONCENT.N

== At the end of the two sequences continue as follows:

g - One card as follows:

## OUTPUT BATCH DATA ##

h - One card, format I10, with the number NBATCH, of output batches.

i - One card as follows:

N    MASS            MASS-SD    \_\_\_\_\_    \_\_\_\_\_SD

In the underlined fields the name of the tracer isotope (see c-) must be inserted twice.

j - NBATCH cards, format 4F10.4. Every card contains, in the order, the following information of the output batch: (J=1,NBATCH)

- . M (J), as described in paragraph 3.1.
- . Experimental standard error of M(J)
- . X(J), as described in paragraph 3.1.
- . Experimental standard deviation of X(J).

k - One card as follows:

## STATISTICAL ANALYSIS INPUT DATA ##

l - One card, format I10, containing an integer odd number for the initialization of the routine SETRAND.

m - One card, format F10.0, containing an integer odd number for the initialization of the routine RANDU.

n - One card, format I10, containing the number of the histories for the Monte Carlo procedure.



o - One card, format 2F10.0, with QMS and DM:

QMS = range, expressed in the mass units, in which the pdf will be calculated.

DM = step length, expressed in mass units, in which the histogram of the pdf will be determined.

Note that the QMS/DM cannot exceed 60.

p - One card, format I10, with NCL, the number of predetermined probability values for which the error limit is requested (NCL ≤ 20).

q - As many cards are necessary to write, with format 5F10.0, the NCL probability values, P(I), mentioned under p-. The P(I) values must be written in increasing order.

r - One card containing the figure 777 (starting from column 8) if punched cards with the pdf histogram are required. Any other number (or a blank card) means that punched results are not required.

### 3.3. Output description

The output of the CC2 code provides the following information.

- A series of tables containing the input data (Relevant parameters of the input and output batches).
- The values of  $H_2$ , calculated according to formula (1)
- The following information on  $H_2$ , interpreted as a random variable:
  - . histogram of the frequencies
  - . histogram and rough plot of the derived pdf
  - . histogram and rough plot of the distribution function
  - . table with the relevant data of the statistical analysis
  - . table for the definition of the error limits at prescribed confidence levels: they are the values  $X_I$  solutions of the equation:

$$P(I) = \int^{X_I} \text{pdf}(H_2) dH_2 \quad (2)$$

- On request (see part r of 3.2) a punched deck with the results of the statistical analysis is delivered. This deck may be used as input for the MUF code (see 5.2).



#### 4. THE CODE 'CC3'

##### 4.1. Outline

The code CC3 evaluates the "three component mixture" contribution,  $H_3$ , to the process inventory:

$$H_3 = \sum_{J=1}^{NBATCH} M(J) \frac{T(J)}{D} \quad (3)$$

NBATCH is the number of the output batches taken into account;  $M(J)$  is the mass of fissile material (Pu or U) of the J-th output batch,

$$T(J) = \begin{vmatrix} 1 & 1 & 1 \\ x_J & c_2 & c_3 \\ Y_J & d_2 & d_3 \end{vmatrix}$$

$$D = \begin{vmatrix} 1 & 1 & 1 \\ c_1 & c_2 & c_3 \\ d_1 & d_2 & d_3 \end{vmatrix}$$

$x_J$  and  $Y_J$  are the relative abundances of the first and second tracer in the J-th output batch,  $c_h, d_h$  ( $h = 1, 2, 3$ ) are the relative abundances of the first and second tracer in the three input superbatches.

The code CC3 is very similar to the CC2: the statistical interpretation of  $H_3$  is performed following the same outlines; the Monte Carlo technique is again used; and limits around  $\bar{H}_3$  are estimated for preselected confidence levels.

##### 4.2. Input data list

a - One card, as follows:

## INPUT BATCH DATA ##

== The sequence from b- to f- must be repeat three times. Every run is specific for the input data characterizing one superbatches ( $K = 1, 2, 3$ ).

b - One card, format 20A4, with the superbatch name (e.g. REACTOR TRINO)

c - One card as follows:

BATCH           MASS (      )           CONC.           CONC.

In the four underlined fields the following alphanumeric symbols must be introduced

- . the fissile element name (PU or U)
- . the mass unit (G or KG)
- . the name of the first tracer (e.g. PU-241)
- . the name of the second tracer (e.g. PU-242)

d - One card, format I10, containing NB(K), the number of batches of the K-th superbatch

e - NB(K) cards, format 3F10.0; every card represents on batch and contains, in sequence, the following data:

- . the total mass of the element contained in the batch
- . the total mass of the first tracer in the batch
- . the total mass of the second tracer in the batch.

f - One card, as follows:

== At the end of the three sequences, continue as follows:

g - One card, as follows:

## OUTPUT BATCH DATA ##

h - One card, as follows:

       MASS (      )           CONC.           CONC.

In the underlined fields the same symbols inserted in the c-card must be introduced.

i - One card, as follows:

|     |       |         |         |         |         |         |
|-----|-------|---------|---------|---------|---------|---------|
| NO. | VALUE | ST.DEV. | PERCENT | ST.DEV. | PERCENT | ST.DEV. |
|-----|-------|---------|---------|---------|---------|---------|

j - One card, format I10, with the number NBATCH of output batches.

k - NBATCH cards, format 6F10.4. Every card represents one batch (J=1, NBATCH) and contains the following sequence of data:

- . M (J) (see 4.1.)
- . Standard deviation of M(J)

- .  $x_j$  (see 4.1) expressed in weight %
- . Standard deviation of  $x_j$
- .  $Y_j$  (see 4.1) expressed in weight %
- . Standard deviation of  $Y_j$

== The final group of input data cards is identical to that of CC2 (from item K- to item r- of paragraph 3.2). Also the meaning of the variables is the same, so that this sequence is not repeated here.

#### 4.3. Output description

The output of the CC3 code provides the following information:

- A series of tables containing the input data (Relevant parameters of input and output batches)
- The value of  $H_3$ , calculated according to formula (3)
- The following information on  $H_3$ , interpreted as a random variable:
  - . relevant data of the pdf of  $H_3$
  - . table for the definition of the error limits at prescribed confidence levels (see 3.3)
  - . histogram of the frequencies
  - . histogram and rough plot of the pdf
  - . histogram and rough plot of the distribution function.
- On request, a punched deck with the results of the statistical analysis is delivered. This deck may be used as input for the MUF code (see 5.2).

## 5. THE CODE 'MUF'

### 5.1. Outline

The DPID supply one of the two terms for the determination of the Material Unaccounted For (MUF). This term is the value of the physical inventory:

$$PI = H_1 + H_2 (+ H_3) \quad (4)$$

The PI is the sum of the two (or three) terms  $H_j$ , the "j-component" mixture contribution (for  $H_2$  and  $H_3$  see respectively ch. 3 and 4).

The MUF is defined by the relationship:

$$MUF = BI - PI \quad (5)$$

where BI is the value of the inventory, as obtained from the accountings for inputs and outputs (Book Inventory).

As far as all the involved parameters can be interpreted as random realizations of unknown quantities, it is possible to define, for each of them, a pdf (the pdf.s of  $H_1$  and BI are assumed to be normal; the ones of  $H_2$  and  $H_3$  are calculated, as histograms, by the codes CC2 and CC3; analytical expressions are not available).

The calculation of the pdf and of the distribution of PI and MUF is obtained by convolutions of the type here described.

Let p and q be independent random variables and  $f_1$  and  $f_2$  the corresponding pdf.s. The analytical expressions for the pdf.s of the random variables:

$$s = p+q$$

$$r = p-q$$

are given, respectively by the following convolution integrals:

$$g(s) = \int f_1(t) \cdot f_2(s-t) dt$$

$$h(r) = \int f_1(r+t) \cdot f_2(t) dt$$



As far as, in the present case the  $f$  are, or may be expressed, in form of histograms, the above integrals are discretized as follows:

$$G(S) = \sum_{K=K_1}^{K_2} F_1(K) \cdot F_2(S-K) \quad (6)$$

$$H(R) = \sum_{J=J_1}^{J_2} F_1(R+J) \cdot F_2(J)$$

(The capital letters used for the function names and variables corresponds to the small letters, which indicate continuous function and variables).

Let  $N_{11}, N_{12}$  ( $N_{11} < N_{12}$ ) define the integer interval outside which  $F_1$  is identically zero and let  $N_{21}, N_{22}$  ( $N_{21} < N_{22}$ ) have the same meaning for  $F_2$ . From these limits it is possible to deduce analogous intervals for the functions  $G$  and  $H$ :

$$N_{11} + N_{21} < S < N_{12} + N_{22}$$

$$N_{11} - N_{22} < R < N_{12} - N_{21}$$

It is useless to include in the sums (6) those terms that certainly do not give any contribution, the sum limits results defined then as follows:

$$K_1 = \text{Max} (N_{11}, S - N_{22})$$

$$K_2 = \text{min} (N_{12}, S - N_{21})$$

$$J_1 = \text{Max} (N_{21}, N_{11} - R)$$

$$J_2 = \text{min} (N_{22}, N_{12} - R)$$

The MUF code makes use of these relationships to calculate the pdf.s, which are associated to the values of PI and MUF, as obtained by (4) and (5).

Actually this code may be used in a more general way: it calculates the pdf of any random variable, when

- a) The random variable is an algebraic sum of independent random variables
- b) The pdf.s of these independent random variables are known.

The calculation is performed as a sequence of convolutions: a first pdf, relative to the random variable  $v_1$  is defined; a second pdf, relative to the random variable  $v_2$  is defined, together with the operation that must be executed on the variables themselves ( $v_1 + v_2$ ,  $v_1 - v_2$ ,  $v_2 - v_1$ ). The program calculates the pdf of the sum and considers it as a new  $v_1$ , so that the sequence can be continued as far as necessary.

The code operates on pdf.s defined in form of histograms, so that the following remarks must be made:

- the histograms of the various pdf.s must have an unique value of the step lenght, PASSO (equal to the DM of codes CC2 and CC3).
- When the pdf of a variable is normal, and is defined by a mean value and a standard deviation, the code converts this continuous function in a histogram with the preselected value of the step. The range  $\pm 3 \sigma$  is considered.

For every convolution performed the code prints: the resulting pdf, with its relevant data and, on request, a rough plot and particular values of the distribution function for the definition of the error limits at preselected confidence levels.

## 5.2. Input data list

- a - One card, format F10.0, with the value of PASSO.
- b - One card, format I10, with the number of preselected values, P(I), for which a value of the resulting random variable must be calculated.
- c - As many cards are necessary to write, with a format 5F10.0 and in ascending order the values of P(I).
- d - A group of cards which define the pdf of the first variable,  $v_1$ , this sequence of cards is described at the end of this paragraph.

e - One card, format 1A3, chosen among the following:

+ The operation between the random variables  $v_1$  (defined above) and  $v_2$  (defined in the following) is  $v_1 + v_2$

1-2 The operation is  $v_1 - v_2$

2-1 The operation is  $v_2 - v_1$

ALT No more convolutions are required.

f - One card, format I10. When it contains the integer 777, it means that the error limits defined by cards b - and c - are requested.

Any other integer number can be introduced when no request in this sense is made.

g - One card, format I10. When it contains the integer 888, it means that a rough plot of the resulting pdf and distribution function are requested. Otherwise any other number (or blank) must be written.

h - A group of cards, identical to the group mentioned as item d -, which defines the pdf of the variable  $v_2$ . The details are given in the following.

== Here a loop begins, because the variable  $v_1$  is now redefined, by the program, as result of the operation performed. A new group of cards, from item e - on, must be inserted, and they describe a new convolution, except when a ALT appears as card of e - type. In this case this is the last card of the input deck.

=== Sequence of cards for the definition of the pdf of a random variable:

i. One card, format I10, with the number, N, of the points in which the pdf of the variable is tabulated. When  $N = 999$  it means that the variable has a normal distribution and that only the card iv must follow.

ii. One card, format 3F10.0, with the following three figures.

. central abscissa of the first step of the given histogram

- . mean value of the variable
  - . standard deviation of the pdf. This last value is not used for computations, but only registered as a relevant parameter of the function.
- iii. A group of cards, as necessary, format 5F12.0, to write the N values of the histogram (end of the sequence).
- iv. One card to be used after card 1. when  $N = 999$ .  
Format 2F10.0. It contains:
- . The mean value and
  - . the standard deviation of the pdf (end of the sequence).

### 5.3. Output description

For every convolution the following output is given:

- a table with
  - . the relevant data and the histogram of the pdf of the first variable
  - . the relevant data and the histogram of the pdf of the second variable
  - . the type of operation performed between the two variables (+, 1-2, 2-1).

Note that from the second convolution on, the first variable is the one resulting from the preceding operation.

- A table with
  - . the resulting pdf
  - . the resulting distribution function
  - . a list of the relevant data of the resulting pdf.
- A table (optional) with the error limits at prescribed confidence levels.
- Two rough plots (optional) of the pdf and of the distribution function.



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```

C
C
C
C
0001 IMPLICIT REAL*8(A-E,G,O-Z)
0002 DIMENSION NAMF(2,10),IDENT(100,4)
0003 DIMENSION GU(100,5),GP(100,5),P(100,10),A(100,10),B(100,10)
0004 DIMENSION TU(100),TP(100),B1(10),B2(10),PUUR(100)
0005 DIMENSION KKK(50,10),JJJ(50,10),LL(100),KK(100)
0006 DIMENSION X(100,2)

C
C
0007 FORMATS
0008 WRITE (6,215)
0009 101 FORMAT(5I10)
0010 102 FORMAT(5F10,C)
0011 104 FORMAT(20A4)
0012 105 FORMAT(10F6,C,I4,4A4)

C
0013 DIMENSION FMT0(20)
0014 READ (5,104) FMT0
0015 300 FORMAT(1H,' FMT0 ',20A4)
0016 WRITE (6,300) FMT0
0017 DIMENSION FMT1(20)
0018 READ (5,104) FMT1
0019 301 FORMAT(1H,' FMT1 ',20A4)
0020 WRITE (6,301) FMT1
0021 202 FORMAT(1H,' HOMOGENEIZATION ACCORDING ISOTOPE ***',2A4,' ***',///)
0022 DIMENSION FMT3(20)
0023 READ (5,104) FMT3
0024 303 FORMAT(1H,' FMT3 ',20A4)
0025 WRITE (6,303) FMT3
0026 DIMENSION FMT4(20)
0027 READ (5,104) FMT4
0028 304 FORMAT(1H,' FMT4 ',20A4)
0029 WRITE (6,304) FMT4
0030 DIMENSION FMT5(20)
0031 READ (5,104) FMT5
0032 305 FORMAT(1H,' FMT5 ',20A4)
0033 WRITE (6,305) FMT5
0034 DIMENSION FMT6(20)
0035 READ (5,104) FMT6
0036 306 FORMAT(1H,' FMT6 ',20A4)
0037 WRITE (6,306) FMT6
0038 DIMENSION FMT7(20)
0039 READ (5,104) FMT7

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0039 307 FORMAT (1H, ' FMT7 ', 20A4)
0040 WRITE (6,307) FMT7
0041 DIMENSION FMT8(20)
0042 READ (5,104) FMT8
0043 308 FORMAT (1H, ' FMT8 ', 20A4)
0044 WRITE (6,308) FMT8
0045 209 FORMAT (1H1, ' ERRORE NEI DATI *** NELEM1,NB1 = ', 2I4)
0046 210 FORMAT (16X, 'LIST OF REJECTED ELEMENTS', //)
0047 211 FORMAT (///, 16X, 'FIRST SUPERBATCH', //)
0048 212 FORMAT (///, 16X, 'SECOND SUPERBATCH', //)
0049 213 FORMAT (1H1)
0050 214 FORMAT (1H1, 12X, '** DATA OF THE PROBLEM **', //, //,
1 TOTAL NUMBER OF AVAILABLE ELEMENTS , 15, //,
2 NUMBER OF ELEMENTS PER DISSOLUTION , 15, //,
3 NUMBER OF BATCHES IN FIRST SUPERBATCH , 15, //,
4 NUMBER OF BATCHES IN SECOND SUPERBATCH , 15, //,
5 NUMBER OF URANIUM ISOTOPES CONSIDERED , 15, //,
6 NUMBER OF PLUTONIUM ISOTOPES CONSIDERED , 15, //,
7 RATIO PU-WEIGHT-UNIT/U-WEIGHT-UNIT , F6.0, //, //)
0051 215 FORMAT (12X, '** VARIABLE FORMAT LIST **', //)
0052 216 FORMAT (' ELEMENTS ORDERED ACCORDING ENCREASING CONCENTRATION OF
1 THE SELECTED ISOTOPE', 2A4, //)
C
C RFAD DATA
C
0053 READ (5,101) NELEM, NB1, NB2, MM
0054 NELEM1=NB1*MM
0055 NELEM2=NB2*MM
0056 AL=MM
0057 READ (5,101) ISU, ISP
0058 READ (5,102) FACTOR
0059 WRITE (6,214) NELEM, MM, NB1, NB2, ISU, ISP, FACTOR
0060 NIS=ISU+ISP
0061 FACTOR=100./FACTOR
0062 READ (5,104) ((NAME(I,K), I=1,2), K=1, NIS)
0063 ITT=10-ISU
0064 AIS=NIS
0065 WRITE (6, FMT0) ((NAME(I,K), I=1,2), K=1, NIS)
C
C
C DO 8 IX=1, NELEM
0066 READ (5,105) ((GU(IX, IU), IU=1, ISU), (GP(IX, IP), IP=1, ITT),
0067 1KK(IX), (IDENT(IX, IT), IT=1, 4))
0068 WRITE (6, FMT1) ((GU(IX, IU), IU=1, ISU), (GP(IX, IP), IP=1, ISF),
1KK(IX), (IDENT(IX, IT), IT=1, 4))
C
C DETERMINATION OF THE ISOTOPIC CONCENTRATIONS

```

```

0069 C TU(IX)=0.
0070 TP(IX)=0.
0071 DO 4 IS=1,ISU
0072 TU(IX)=TU(IX)+GU(IX,IS)
0073 4 CONTINUE
0074 DO 5 IS=1,ISP
0075 TP(IX)=TP(IX)+GP(IX,IS)
0076 5 CONTINUE
0077 PUUR(IX)=(TP(IX)/TU(IX))*FACTOR
0078 DO 6 IS=1,ISU
0079 P(IX,IS)=GU(IX,IS)/TU(IX)
0080 6 CONTINUE
0081 DO 7 IS=1,ISP
0082 ISS=ISU+IS
0083 P(IX,ISS)=GP(IX,IS)/TP(IX)
0084 7 CONTINUE
0085 8 CONTINUE
0086 WRITE (6,213)
0087 WRITE (6,FMT3) ((NAME(I,K),I=1,2),K=1,NIS)
0088 DO 2 IX=1,NELEM
0089 WRITE (6,FMT8) (IX,(IDENT(IX,IT),IT=1,4),(P(IX,IS),IS=1,NIS),
0090 1PUUR(IX))
0090 2 CONTINUE

 C
 C
 C OMOGENIZATION ACCORDING ISOTOPE 'ISS'
 C
0091 DO 999 ISS=1,NIS
 C
0092 DO 9 IS=1,10
0093 B1(IS)=0.
0094 B2(IS)=0.
0095 DO 9 J=1,100
0096 B(J,IS)=0.
0097 9 CONTINUE
 C
0098 WRITE (6,202) (NAME(I,ISS),I=1,2)
 C
 C
 C ORDERING OF FUELS ACCORDING ENCREASING CONCENTRATION OF 'ISS'
 C
0099 DO 10 IX=1,NELEM
0100 X(IX,1)=P(IX,ISS)
0101 X(IX,2)=FLOAT(IX)
0102 10 CONTINUE
0103 CALL NDOR2(NELEM,X)
 C
0104 WRITE (6,216) (NAME(I,ISS),I=1,2)

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```

0105 WRITE (6,FMT3) ((NAME(I,K),I=1,2),K=1,NIS)
0106 DO 31 J=1,NELEM
0107 I=X(J,2)
0108 WRITE (6,FMT4) (J,(IDENT(I,IT),IT=1,4),(P(I,IS),IS=1,NIS))
0109 31 CONTINUE

C
C
C SUPERBATCH NUMBER 1
C
0110 WRITE (6,213)
C
0111 IF (NELEM1.EQ.0) GO TO 60
0112 N01=NELEM-NELEM2
0113 IF (NELEM1.GT.N01) GO TO 70
0114 IF (NELEM1.EQ.N01) GO TO 15
0115 N00=NELEM1+1
0116 WRITE (6,210)
0117 WRITE (6,FMT3) ((NAME(I,K),I=1,2),K=1,NIS)
0118 DO 72 IX=N00,N01
0119 I=X(IX,2)
0120 LL(IX)=I
0121 K=IX-N00+1
0122 WRITE (6,FMT4) (K,(IDENT(I,IT),IT=1,4),(P(I,IS),IS=1,NIS))
0123 72 CONTINUE
0124 15 CONTINUE

C
C
C FUEL DATA TRANSFERRED IN WORK MATRIX 'A'
C
0125 DO 14 IX=1,NELEM1
0126 I=X(IX,2)
0127 LL(IX)=I
0128 DO 12 IS=1,NIS
0129 A(IX,IS)=P(I,IS)
0130 12 CONTINUE
0131 14 CONTINUE

C
0132 CALL SUPBCH(NELEM1,A,LL,KKK,NB1,NIS,B,ISS)
C
C
C FINAL BATCH COMPOSITIONS
C
0133 WRITE (6,211)
0134 WRITE (6,FMT3) ((NAME(I,K),I=1,2),K=1,NIS)
0135 DO 62 J=1,NB1
0136 DO 50 I=1,MM
0137 K=KKK(J,I)
0138 WRITE (6,FMT4) (K,(IDENT(K,IT),IT=1,4),(P(K,IS),IS=1,NIS))
0139 50 CONTINUE
0140 DO 54 IS=1,NIS
0141 B(J,IS)=B(J,IS)/AL

```

```

0142 B1(IS)=B1(IS)+B(J,IS)
0143 B2(IS)=B2(IS)+B(J,IS)*B(J,IS)
0144 54 CONTINUE
0145 WRITE (6,FMT5) (J,(B(J,IS),IS=1,NIS))
0146 62 CONTINUE
C
C SUPERBATCH CHARACTERISTICS
C
0147 BB1=NB1
0148 DO 66 IS=1,NIS
0149 B1(IS)=B1(IS)/BB1
0150 B2(IS)=DSQRT((B2(IS)-BB1*B1(IS)*B1(IS))/(BB1-1.))
0151 66 CONTINUE
0152 WRITE (6,FMT6) (B1(IS),IS=1,NIS)
0153 WRITE (6,FMT7) (B2(IS),IS=1,NIS)
C
0154 60 CONTINUE
C
0155 IF (NELEM2.EQ.0) GO TO 999
C
C SUPERBATCH NUMBER 2
C
0156 NO3=NELEM-NELEM2
0157 IF (NELEM1.NE.0) GO TO 87
0158 WRITE (6,210)
0159 WRITE (6,FMT3) ((NAME(I,K),I=1,2),K=1,NIS)
0160 DO 61 IX=1,NO3
0161 I=X(IX,2)
0162 LL(IX)=I
0163 K=IX
0164 WRITE (6,FMT4) (K,(IDENT(I,IT),IT=1,4),(P(I,IS),IS=1,NIS))
0165 61 CONTINUE
0166 87 CONTINUE
C
0167 DO 48 IS=1,10
0168 B1(IS)=0.
0169 B2(IS)=0.
0170 DO 48 J=1,100
0171 B(J,IS)=0.
0172 48 CONTINUE
C
C FUEL DATA TRANSFERRED IN WORK MATRIX 'A'
C
0173 DO 80 IX=1,NELEM2
0174 NO4=NO3+IX
0175 I=X(NO4,2)
0176 LL(IX)=I
0177 DO 80 IS=1,NIS

```

```

0178 A(IX,IS)=P(I,IS)
0179 80 CONTINUE
 C
0180 CALL SUPBCH(NELEM2,A,LL,KKK,NB2,NIS,B,ISS)
 C
 C SECOND SUPERBATCH CHARACTERISTICS
 C
0181 WRITE (6,212)
0182 WRITE (6,FMT3) ((NAME(I,K),I=1,2),K=1,NIS)
0183 DO 63 J=1,NB2
0184 DO 51 I=1,MM
0185 K=KKK(J,I)
0186 WRITE (6,FMT4) (K,(IDENT(K,IT),IT=1,4),(P(K,IS),IS=1,NIS))
0187 51 CONTINUE
0188 DO 55 IS=1,NIS
0189 B(J,IS)=B(J,IS)/AL
0190 B1(IS)=B1(IS)+B(J,IS)
0191 B2(IS)=B2(IS)+B(J,IS)*B(J,IS)
0192 55 CONTINUE
0193 WRITE (6,FMT5) (J,(B(J,IS),IS=1,NIS))
0194 63 CONTINUE
 C
 C SUPERBATCH CHARACTERISTICS
 C
0195 BB2=NB2
0196 DO 67 IS=1,NIS
0197 B1(IS)=B1(IS)/BB2
0198 B2(IS)=DSQRT((B2(IS)-BB2*B1(IS)*B1(IS))/(BB2-1.))
0199 67 CONTINUE
0200 WRITE (6,FMT6) (B1(IS),IS=1,NIS)
0201 WRITE (6,FMT7) (B2(IS),IS=1,NIS)
 C
0202 999 CONTINUE
 C
0203 GO TO 1000
0204 70 CONTINUE
0205 WRITE (6,209) NELEM1,N01
0206 1000 CONTINUE
0207 STOP
0208 END

```

```
0001 C SUBROUTINE NDOR2(N,X)
0002 IMPLICIT REAL*8(A-H,O-Z)
0003 DIMENSION X(100,2)
0004 C
0005 DO 5 I=2,N
0006 IF(X(I,1)-X(I-1,1)) 1,5,5
0007 1 TEMP1=X(I,1)
0008 TEMP2=X(I,2)
0009 IM1=I-1
0010 DO 3 J=1,IM1
0011 L=I-J
0012 IF(TEMP1-X(L,1)) 2,4,4
0013 2 X(L+1,1)=X(L,1)
0014 X(L+1,2)=X(L,2)
0015 3 CONTINUE
0016 X(1,1)=TEMP1
0017 X(1,2)=TEMP2
0018 GO TO 5
0019 4 X(L+1,1)=TEMP1
0020 X(L+1,2)=TEMP2
0021 5 CONTINUE
0022 C RETURN
0023 END
```



125

LIST OF THE DATA CAPDS USED FOR THE 'ORDER' SAMPLE PROGRAM

```

(1H,16X,'REACTOR DATA',////,6(2X,2A4),' FUEL EL. IDENT.',//)
(6F10.3,I4,4A4)
(RX,'FUEL ELEMENT IDENT.',6(2A4,1X),//)
(' ',I10,4A4,6F0.5)
(/,' BATCH',I3,18X,6F9.5,//)
(1H,////,' SUPERBATCH MEAN VALUES ',6F0.5)
(13X,' STAND. DEV. ',6F0.5)
(' ',I10,4A4,6F9.5,' PU/U RATIO PERCENT='F7.5)

```

| 136   | U-235 | U-236 | U-238 | PU-239 | PU-240 | PU 241 |
|-------|-------|-------|-------|--------|--------|--------|
| 186.5 | 27.30 | 7966. | 4565. | 9620.  | 527.2  |        |
| 177.6 | 30.22 | 7943. | 4790. | 1092.  | 675.6  |        |
| 168.8 | 30.36 | 7942. | 4795. | 1100.  | 683.4  |        |
| 121.5 | 26.57 | 7996. | 4767. | 1286.  | 727.0  |        |
| 122.1 | 26.47 | 7997. | 4771. | 1277.  | 721.2  |        |
| 123.3 | 26.26 | 7999. | 4737. | 1265.  | 703.5  |        |
| 122.1 | 26.46 | 7997. | 4758. | 1279.  | 719.2  |        |
| 124.7 | 26.02 | 8001. | 4723. | 1253.  | 693.4  |        |
| 122.4 | 26.43 | 7997. | 4768. | 1278.  | 719.6  |        |
| 123.6 | 26.72 | 7995. | 4789. | 1290.  | 734.6  |        |
| 118.5 | 27.05 | 7991. | 4816. | 1314.  | 760.5  |        |
| 124.1 | 26.14 | 8000. | 4735. | 1256.  | 695.8  |        |
| 116.8 | 27.34 | 7989. | 4958. | 1333.  | 785.2  |        |
| 116.7 | 27.32 | 7989. | 4836. | 1330.  | 779.5  |        |
| 115.7 | 27.50 | 7987. | 4857. | 1346.  | 796.1  |        |
| 121.2 | 26.76 | 7994. | 4750. | 1300.  | 743.5  |        |
| 116.4 | 27.40 | 7988. | 4862. | 1338.  | 790.2  |        |
| 114.9 | 27.63 | 7986. | 4868. | 1355.  | 806.5  |        |
| 117.7 | 27.17 | 7991. | 4825. | 1319.  | 767.8  |        |
| 122.0 | 26.47 | 7997. | 4770. | 1280.  | 722.2  |        |
| 116.6 | 27.35 | 7989. | 4844. | 1329.  | 780.8  |        |
| 115.6 | 27.51 | 7987. | 4860. | 1342.  | 795.5  |        |
| 117.1 | 27.27 | 7989. | 4838. | 1323.  | 774.2  |        |
| 116.7 | 27.32 | 7989. | 4843. | 1327.  | 778.8  |        |
| 126.0 | 25.81 | 8003. | 4701. | 1238.  | 677.1  |        |
| 129.0 | 25.29 | 8007. | 4639. | 1203.  | 640.1  |        |
| 126.4 | 25.73 | 8003. | 4693. | 1233.  | 671.7  |        |
| 122.7 | 26.37 | 7998. | 4762. | 1274.  | 715.5  |        |
| 174.3 | 26.57 | 7947. | 4720. | 106.   | 637.0  |        |
| 173.6 | 26.76 | 7946. | 4734. | 1066.  | 644.5  |        |
| 171.6 | 30.04 | 7944. | 4765. | 1084.  | 664.5  |        |
| 122.7 | 26.49 | 7997. | 4774. | 1282.  | 723.7  |        |
| 115.5 | 27.53 | 7997. | 4861. | 1344.  | 706.5  |        |
| 118.3 | 27.06 | 7991. | 4819. | 1311.  | 759.5  |        |
| 120.8 | 26.66 | 7995. | 4783. | 1292.  | 735.5  |        |
| 171.5 | 30.07 | 7944. | 4768. | 1085.  | 666.0  |        |
| 171.3 | 30.09 | 7943. | 4776. | 1086.  | 667.9  |        |
| 170.6 | 30.21 | 7943. | 4782. | 1093.  | 674.8  |        |
| 116.9 | 27.29 | 7989. | 4845. | 1327.  | 778.8  |        |
| 114.1 | 27.77 | 7985. | 4895. | 1363.  | 819.6  |        |

|      |          |     |     |
|------|----------|-----|-----|
| 1    | *509-129 | F12 | 129 |
| 1    | *509-111 | D12 | 49  |
| 1    | *509-117 | J09 | 59  |
| 1    | 509-076  | F04 | 94  |
| 2    | 509-058  | E05 | 88  |
| 2    | 509-074  | H04 | 109 |
| 2    | 509-078  | G09 | 107 |
| 2    | 509-052  | I07 | 117 |
| 3    | 509-043  | H02 | 113 |
| 3    | 509-059  | I04 | 68  |
| 3    | 509-061  | J04 | 65  |
| 3    | 509-054  | D08 | 86  |
| 4    | 509-044  | I09 | 58  |
| 4    | 509-048  | C08 | 45  |
| 4    | 509-064  | G10 | 108 |
| 4    | 509-073  | J06 | 119 |
| 5    | 509-063  | C05 | 80  |
| 5    | 509-047  | F03 | 93  |
| 5    | 509-050  | E09 | 92  |
| 5    | 509-055  | H06 | 111 |
| 6    | 509-072  | F06 | 96  |
| 6    | 509-062  | E10 | 50  |
| 6    | 509-075  | F08 | 98  |
| 6    | 509-071  | G07 | 105 |
| 7    | 509-051  | H10 | 55  |
| 7    | 509-057  | I05 | 115 |
| 7    | 509-053  | E03 | 75  |
| 7    | 509-067  | D06 | 84  |
| 8    | *509-116 | J03 | 66  |
| 8    | *509-112 | J03 | 66  |
| 8    | *509-114 | D03 | 79  |
| 8    | 509-046  | G05 | 103 |
| 9    | 509-042  | H03 | 70  |
| 9    | 509-045  | E07 | 90  |
| 9    | 509-065  | C07 | 82  |
| 10   | *509-118 | C04 | 79  |
| 10   | *509-115 | C09 | 46  |
| 10   | *509-113 | I10 | 56  |
| 1000 | 509-069  | D04 | 78  |
| 1000 | 509-041  | J08 | 60  |

**\*\* VARIABLE FORMAT LIST \*\***

```

FMT0 (1H,16X,'REACTOR DATA',////,6(2X,2A4), ' FUEL EL. IDENT.',/)
FMT1 (6F10.3,14,4A4)
FMT3 (8X,'FUEL ELEMENT IDENT.', 6(2A4,1X),/)
FMT4 (' ',110,4A4, 6F9.5)
FMT5 (' ', ' BATCH',13,18X, 6F9.5,/)
FMT6 (1H,///, ' SUPERPATCH MEAN VALUES ',6F9.5)
FMT7 (13X,'STAND. DEV.', 6F9.5)
FMT8 (' ',110,4A4, 6F9.5, ' PU/U RATIO PERCENT= 'F7.5)

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\*\* DATA OF THE PROBLEM \*\*

TOTAL NUMBER OF AVAILABLE ELEMENTS  
 NUMBER OF ELEMENTS PER DISSOLUTION  
 NUMBER OF BATCHES IN FIRST SUPERBATCH  
 NUMBER OF BATCHES IN SECOND SUPERBATCH  
 NUMBER OF URANIUM ISOTOPES CONSIDERED  
 NUMBER OF PLUTONIUM ISOTOPES CONSIDERED  
 RATIO PU-WEIGHT-UNIT/U-WEIGHT-UNIT

4  
 1000  
 1000  
 1000  
 1000  
 1000  
 1000

REACTOR DATA

| U-235   | U-236  | U-238    | PU-239   | PU-240   | PU 241  | FUEL EL. IDENT.        |
|---------|--------|----------|----------|----------|---------|------------------------|
| 186.500 | 27.390 | 7960.000 | 4505.000 | 962.000  | 527.200 | 1*509-109 F10 100      |
| 177.600 | 37.220 | 7943.000 | 4790.000 | 1092.000 | 675.600 | 1*509-111 D10 49       |
| 169.800 | 30.360 | 7942.000 | 4795.000 | 1100.000 | 683.400 | 1*509-117 J09 59       |
| 121.500 | 26.570 | 7996.000 | 4767.000 | 1286.000 | 727.000 | 1 509-076 F04 94       |
| 122.100 | 26.470 | 7997.000 | 4771.000 | 1277.000 | 721.200 | 2 509-058 E05 88       |
| 123.300 | 26.260 | 7995.000 | 4737.000 | 1265.000 | 703.500 | 2 509-074 H04 109      |
| 122.100 | 26.460 | 7997.000 | 4758.000 | 1279.000 | 719.200 | 2 509-078 G09 107      |
| 124.700 | 26.020 | 8001.000 | 4723.000 | 1253.000 | 693.400 | 2 509-052 I07 117      |
| 122.400 | 26.430 | 7997.000 | 4768.000 | 1278.000 | 719.600 | 3 509-043 H08 113      |
| 120.600 | 26.720 | 7995.000 | 4789.000 | 1290.000 | 734.600 | 3 509-059 I04 68       |
| 118.500 | 27.050 | 7991.000 | 4816.000 | 1314.000 | 760.500 | 3 509-061 J04 65       |
| 124.100 | 26.140 | 8000.000 | 4735.000 | 1256.000 | 695.800 | 3 509-054 D08 86       |
| 116.800 | 27.340 | 7989.000 | 4858.000 | 1333.000 | 785.200 | 4 509-044 I09 58       |
| 116.700 | 27.320 | 7989.000 | 4836.000 | 1330.000 | 779.500 | 4 509-048 C08 45       |
| 115.700 | 27.500 | 7987.000 | 4857.000 | 1346.000 | 796.100 | 4 509-064 G10 108      |
| 120.200 | 26.760 | 7994.000 | 4790.000 | 1300.000 | 743.500 | 4 509-073 J06 119      |
| 116.400 | 27.400 | 7988.000 | 4862.000 | 1338.000 | 790.200 | 5 509-063 C05 80       |
| 114.900 | 27.630 | 7986.000 | 4868.000 | 1355.000 | 806.500 | 5 509-047 F03 93       |
| 117.700 | 27.170 | 7991.000 | 4825.000 | 1319.000 | 767.800 | 5 509-050 F09 92       |
| 122.000 | 26.470 | 7997.000 | 4770.000 | 1280.000 | 722.200 | 5 509-055 H06 111      |
| 116.600 | 27.350 | 7989.000 | 4844.000 | 1329.000 | 780.800 | 6 509-072 F06 96       |
| 115.600 | 27.510 | 7987.000 | 4860.000 | 1342.000 | 795.500 | 6 509-062 F10 50       |
| 117.100 | 27.270 | 7985.000 | 4836.000 | 1323.000 | 774.200 | 6 509-075 F08 98       |
| 116.700 | 27.320 | 7989.000 | 4843.000 | 1327.000 | 778.800 | 6 509-071 G07 105      |
| 126.000 | 25.810 | 8003.000 | 4701.000 | 1238.000 | 677.100 | 7 509-051 H10 55       |
| 129.000 | 25.290 | 8007.000 | 4635.000 | 1203.000 | 640.100 | 7 509-057 I05 115      |
| 126.400 | 25.730 | 8003.000 | 4693.000 | 1233.000 | 671.700 | 7 509-053 F03 75       |
| 122.700 | 26.370 | 7998.000 | 4762.000 | 1274.000 | 715.500 | 7 509-067 D06 84       |
| 174.300 | 29.570 | 7947.000 | 4720.000 | 1065.000 | 637.000 | 8*509-116 J03 66       |
| 173.600 | 29.700 | 7946.000 | 4734.000 | 1066.000 | 644.500 | 8*509-112 I03 69       |
| 171.600 | 30.040 | 7944.000 | 4765.000 | 1084.000 | 664.500 | 8*509-114 D03 76       |
| 122.000 | 26.450 | 7997.000 | 4774.000 | 1282.000 | 723.700 | 8 509-046 G05 103      |
| 115.500 | 27.530 | 7987.000 | 4861.000 | 1344.000 | 796.900 | 9 509-042 H03 70       |
| 118.300 | 27.060 | 7991.000 | 4815.000 | 1311.000 | 759.500 | 9 509-045 E07 90       |
| 120.800 | 26.660 | 7995.000 | 4783.000 | 1292.000 | 735.500 | 9 509-065 C07 82       |
| 171.500 | 30.070 | 7944.000 | 4768.000 | 1085.000 | 666.000 | 10*509-118 C04 79      |
| 171.300 | 30.090 | 7943.000 | 4776.000 | 1086.000 | 667.900 | 10*509-115 C09 46      |
| 170.600 | 30.210 | 7943.000 | 4782.000 | 1093.000 | 674.800 | 10*509-113 I10 56      |
| 116.900 | 27.290 | 7989.000 | 4845.000 | 1327.000 | 778.800 | 1000. 509-069. D04. 78 |

114.100 27.770 7985.000 4895.000 1363.000 819.6001000.509-041 J08..60

FUEL ELEMENT IDENT. U-235 U-236 U-238 PU-239 PU-240 PU 241

|     |         |     |     |         |         |         |         |         |         |      |       |           |         |
|-----|---------|-----|-----|---------|---------|---------|---------|---------|---------|------|-------|-----------|---------|
| 1*  | 509-109 | F10 | 100 | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 | PU/U | RATIO | PERCENT = | 0.73382 |
| 2*  | 509-111 | D10 | 49  | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 | PU/U | RATIO | PERCENT = | 0.80522 |
| 3*  | 509-117 | J09 | 59  | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 | PU/U | RATIO | PERCENT = | 0.80794 |
| 4*  | 509-076 | F04 | 94  | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 | PU/U | RATIO | PERCENT = | 0.83251 |
| 5*  | 509-058 | F05 | 88  | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 | PU/U | RATIO | PERCENT = | 0.83103 |
| 6*  | 509-074 | H04 | 109 | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 | PU/U | RATIO | PERCENT = | 0.82291 |
| 7*  | 509-078 | G09 | 107 | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 | PU/U | RATIO | PERCENT = | 0.82943 |
| 8*  | 509-052 | I07 | 117 | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 | PU/U | RATIO | PERCENT = | 0.81816 |
| 9*  | 509-043 | H08 | 113 | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 | PU/U | RATIO | PERCENT = | 0.83056 |
| 10* | 509-059 | I04 | 68  | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 | PU/U | RATIO | PERCENT = | 0.83681 |
| 11* | 509-061 | J04 | 65  | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 | PU/U | RATIO | PERCENT = | 0.84686 |
| 12* | 509-054 | D08 | 86  | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 | PU/U | RATIO | PERCENT = | 0.82044 |
| 13* | 509-044 | I09 | 58  | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 | PU/U | RATIO | PERCENT = | 0.85775 |
| 14* | 509-048 | C08 | 45  | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 | PU/U | RATIO | PERCENT = | 0.85399 |
| 15* | 509-064 | G10 | 108 | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 | PU/U | RATIO | PERCENT = | 0.86089 |
| 16* | 509-073 | J06 | 119 | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 | PU/U | RATIO | PERCENT = | 0.83940 |
| 17* | 509-063 | C05 | 80  | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 | PU/U | RATIO | PERCENT = | 0.85961 |
| 18* | 509-047 | F03 | 93  | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 | PU/U | RATIO | PERCENT = | 0.86479 |
| 19* | 509-050 | E09 | 92  | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 | PU/U | RATIO | PERCENT = | 0.84955 |
| 20* | 509-055 | H06 | 111 | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 | PU/U | RATIO | PERCENT = | 0.83141 |
| 21* | 509-072 | F06 | 96  | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 | PU/U | RATIO | PERCENT = | 0.85502 |
| 22* | 509-062 | E10 | 50  | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 | PU/U | RATIO | PERCENT = | 0.86069 |
| 23* | 509-075 | F08 | 98  | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 | PU/U | RATIO | PERCENT = | 0.85268 |
| 24* | 509-071 | G07 | 105 | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 | PU/U | RATIO | PERCENT = | 0.85439 |
| 25* | 509-051 | H10 | 55  | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 | PU/U | RATIO | PERCENT = | 0.81131 |
| 26* | 509-057 | I05 | 115 | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 | PU/U | RATIO | PERCENT = | 0.79425 |
| 27* | 509-053 | F03 | 75  | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 | PU/U | RATIO | PERCENT = | 0.80902 |
| 28* | 509-067 | D06 | 84  | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 | PU/U | RATIO | PERCENT = | 0.82870 |
| 29* | 509-116 | J03 | 66  | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 | PU/U | RATIO | PERCENT = | 0.78728 |
| 30* | 509-112 | I03 | 69  | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 | PU/U | RATIO | PERCENT = | 0.79080 |
| 31* | 509-114 | D03 | 76  | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 | PU/U | RATIO | PERCENT = | 0.79963 |
| 32* | 509-046 | G05 | 103 | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 | PU/U | RATIO | PERCENT = | 0.83233 |
| 33* | 509-042 | E03 | 70  | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 | PU/U | RATIO | PERCENT = | 0.86124 |
| 34* | 509-045 | F07 | 90  | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 | PU/U | RATIO | PERCENT = | 0.84675 |
| 35* | 509-065 | C07 | 82  | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 | PU/U | RATIO | PERCENT = | 0.83642 |
| 36* | 509-118 | C04 | 79  | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 | PU/U | RATIO | PERCENT = | 0.80031 |
| 37* | 509-115 | C09 | 46  | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 | PU/U | RATIO | PERCENT = | 0.80177 |
| 38* | 509-113 | I10 | 56  | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 | PU/U | RATIO | PERCENT = | 0.80427 |
| 39* | 509-069 | D04 | 78  | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 | PU/U | RATIO | PERCENT = | 0.85462 |
| 40* | 509-041 | J08 | 60  | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 | PU/U | RATIO | PERCENT = | 0.87089 |

CMOGENEIZATION ACCORDING ISOTOPE \*\*\* U-235 \*\*\*

ELEMENTS ORDERED ACCORDING INCREASING CONCENTRATION OF THE SELECTED ISOTOPE U-235

| FUEL | ELEMENT | IDENT.   | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|------|---------|----------|---------|---------|---------|---------|---------|---------|
| 1.   | 509-041 | J08. 60  | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
| 2.   | 509-047 | F03. 93  | 0.01414 | 0.00342 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |
| 3.   | 509-042 | H03. 70  | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
| 4.   | 509-062 | E10. 50  | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |
| 5.   | 509-064 | G10. 108 | 0.01423 | 0.00337 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
| 6.   | 509-063 | C05. 80  | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
| 7.   | 509-072 | F06. 96  | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
| 8.   | 509-048 | C08. 45  | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
| 9.   | 509-071 | G07. 105 | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |
| 10.  | 509-044 | I09. 58  | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
| 11.  | 509-069 | D04. 78  | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |
| 12.  | 509-075 | F28. 98  | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| 13.  | 509-050 | E09. 92  | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| 14.  | 509-045 | E07. 90  | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| 15.  | 509-061 | J04. 65  | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| 16.  | 509-073 | J06. 119 | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| 17.  | 509-059 | I04. 68  | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 18.  | 509-065 | C07. 82  | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| 19.  | 509-076 | F04. 94  | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| 20.  | 509-046 | G05. 103 | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| 21.  | 509-055 | F06. 111 | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 22.  | 509-058 | E05. 88  | 0.01496 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| 23.  | 509-078 | G09. 107 | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
| 24.  | 509-043 | H08. 113 | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 25.  | 509-067 | D06. 84  | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| 26.  | 509-074 | H04. 109 | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| 27.  | 509-054 | D08. 86  | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| 28.  | 509-052 | I07. 117 | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| 29.  | 509-051 | H10. 55  | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| 30.  | 509-053 | F03. 75  | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |
| 31.  | 509-057 | I05. 115 | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |
| 32.  | 509-117 | J09. 59  | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |
| 33.  | 509-111 | D10. 49  | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| 34.  | 509-113 | I10. 56  | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
| 35.  | 509-115 | C09. 46  | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |
| 36.  | 509-118 | C04. 79  | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |
| 37.  | 509-114 | D03. 76  | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |
| 38.  | 509-112 | I03. 69  | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 39.  | 509-116 | J03. 66  | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 40.  | 509-109 | F10. 100 | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |

# LIST OF REJECTED ELEMENTS

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1 509-067 D06 84    | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| 2 509-074 H04 109   | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| 3 509-054 D08 86    | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| 4 509-052 I07 117   | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| 5 509-051 H10 55    | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| 6 509-053 E03 75    | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |
| 7 509-057 I05 115   | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |

## FIRST SUPERBATCH

| FUEL ELEMENT IDENT.  | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|----------------------|---------|---------|---------|---------|---------|---------|
| 40. 509-041 J08. 60  | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
| 9 509-043 H08 113    | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 16 509-073 J06 119   | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| BATCH 1              | 0.01461 | 0.00332 | 0.98207 | 0.69911 | 0.19057 | 0.11032 |
| 18 509-047 F03 93    | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |
| 7 509-078 G09 107    | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
| 11 509-061 J04 65    | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| BATCH 2              | 0.01456 | 0.00332 | 0.98211 | 0.69856 | 0.19092 | 0.11052 |
| 14 509-048 C08 45    | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
| 10 509-059 I04 68    | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 34 509-045 E07 90    | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| BATCH 3              | 0.01457 | 0.00332 | 0.98211 | 0.69954 | 0.19037 | 0.11009 |
| 21 509-072 F06 96    | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
| 35 509-065 C07 82    | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| 19 509-050 E09 92    | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| BATCH 4              | 0.01455 | 0.00333 | 0.98213 | 0.69899 | 0.19055 | 0.11045 |
| 33 509-042 H03 70    | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
| 5 509-058 E05 88     | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| 23 509-075 F08 98    | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| BATCH 5              | 0.01453 | 0.00333 | 0.98214 | 0.69888 | 0.19045 | 0.11066 |
| 22 509-062 E10 50    | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |
| 20 509-055 H06 111   | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 39. 509-069. D04. 78 | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |



|            |                    |         |         |         |         |         |         |
|------------|--------------------|---------|---------|---------|---------|---------|---------|
| BATCH 6    |                    | 0.01452 | 0.00333 | 0.98215 | 0.69864 | 0.19057 | 0.11079 |
|            | 15 509-064 G10 108 | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
|            | 32 509-046 G05 103 | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
|            | 13 509-044 I09 58  | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
| BATCH 7    |                    | 0.01452 | 0.00333 | 0.98214 | 0.69816 | 0.19083 | 0.11101 |
|            | 17 509-063 C05 80  | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
|            | 4 509-076 F04 94   | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
|            | 24 509-071 G07 105 | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |
| BATCH 8    |                    | 0.01453 | 0.00333 | 0.98214 | 0.69853 | 0.19068 | 0.11078 |
| SUPERBATCH | MEAN VALUES        | 0.01455 | 0.00333 | 0.98212 | 0.69880 | 0.19062 | 0.11058 |
|            | STAND. DEV.        | 0.00003 | 0.00001 | 0.00003 | 0.00042 | 0.00018 | 0.00029 |

# SECOND SUPERBATCH

|            | FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|------------|---------------------|---------|---------|---------|---------|---------|---------|
|            | 38*509-113 I10 56   | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
|            | 30*509-112 I03 69   | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
|            | 31*509-114 D03 76   | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |
| BATCH 1    |                     | 0.02111 | 0.00368 | 0.97521 | 0.73208 | 0.16624 | 0.10168 |
|            | 2*509-111 D10 49    | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
|            | 29*509-116 J03 66   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
|            | 36*509-118 C04 79   | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |
| BATCH 2    |                     | 0.02113 | 0.00368 | 0.97519 | 0.73247 | 0.16605 | 0.10149 |
|            | 3*509-117 J09 59    | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |
|            | 1*509-109 F10 100   | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
|            | 37*509-115 C09 46   | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |
| BATCH 3    |                     | 0.02157 | 0.00359 | 0.97484 | 0.73734 | 0.16464 | 0.09802 |
| SUPERBATCH | MEAN VALUES         | 0.02127 | 0.00365 | 0.97508 | 0.73396 | 0.16564 | 0.10040 |
|            | STAND. DEV.         | 0.00026 | 0.00005 | 0.00021 | 0.00293 | 0.00088 | 0.00206 |

CMOGENEIZATION ACCORDING ISOTOPE \*\*\* U-236 \*\*\*

ELEMENTS ORDERED ACCORDING INCREASING CONCENTRATION OF THE SELECTED ISOTOPE U-236

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1 509-057 I05 115   | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |
| 2 509-053 E03 75    | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |
| 3 509-051 H10 55    | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| 4 509-052 I07 117   | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| 5 509-054 D08 86    | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| 6 509-074 H04 109   | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| 7 509-067 D06 84    | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| 8 509-043 H08 113   | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 9 509-078 G09 107   | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
| 10 509-058 E05 88   | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| 11 509-055 H06 111  | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 12 509-046 G05 103  | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| 13 509-076 F04 94   | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| 14 509-065 C07 82   | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| 15 509-059 I04 68   | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 16 509-073 J06 119  | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| 17 509-061 J04 65   | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| 18 509-045 E07 90   | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| 19 509-050 E09 92   | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| 20 509-109 F10 100  | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
| 21 509-075 F08 98   | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| 22 509-069 D04 78   | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |
| 23 509-048 C08 45   | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
| 24 509-071 G07 105  | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |
| 25 509-044 I09 58   | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
| 26 509-072 F06 96   | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
| 27 509-063 C05 80   | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
| 28 509-064 G10 108  | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
| 29 509-062 F10 50   | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |
| 30 509-042 H03 70   | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
| 31 509-047 F03 93   | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |
| 32 509-041 J08 60   | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
| 33 509-116 J03 66   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 34 509-112 I03 69   | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 35 509-114 D03 76   | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |
| 36 509-118 C04 79   | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |
| 37 509-115 C09 46   | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |
| 38 509-113 I10 56   | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
| 39 509-111 D10 49   | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| 40 509-117 J09 59   | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |

# LIST OF REJECTED ELEMENTS

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1 509-044 I09 58    | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
| 2 509-072 F06 96    | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
| 3 509-063 C05 80    | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
| 4 509-064 G10 108   | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
| 5 509-062 E10 50    | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |
| 6 509-042 H03 70    | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
| 7 509-047 F03 93    | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |

## FIRST SUPERBATCH

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 26 509-057 I05 115  | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |
| 24 509-071 G07 105  | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |
| 16 509-073 J06 119  | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| BATCH 1             | 0.01497 | 0.00325 | 0.98178 | 0.70453 | 0.18893 | 0.10654 |
| 27 509-053 E03 75   | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |
| 14 509-048 C08 45   | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
| 10 509-059 I04 68   | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| BATCH 2             | 0.01489 | 0.00327 | 0.98185 | 0.70348 | 0.18923 | 0.10728 |
| 25 509-051 H10 55   | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| 39 509-069 D04 78   | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |
| 35 509-065 C07 82   | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| BATCH 3             | 0.01489 | 0.00326 | 0.98185 | 0.70329 | 0.18925 | 0.10746 |
| 8 509-052 I07 117   | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| 23 509-075 F08 98   | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| 4 509-076 F04 94    | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| BATCH 4             | 0.01487 | 0.00327 | 0.98186 | 0.70295 | 0.18944 | 0.10761 |
| 12 509-054 D08 86   | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10436 |
| 1 509-109 F10 100   | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
| 32 509-046 G05 103  | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| BATCH 5             | 0.01767 | 0.00327 | 0.97906 | 0.72133 | 0.17910 | 0.09956 |
| 6 509-074 H04 109   | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| 19 509-050 F09 92   | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| 20 509-055 H06 111  | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 6 |  | 0.01486 | 0.00327 | 0.98187 | 0.70296 | 0.18950 | 0.10755 |
|---------|--|---------|---------|---------|---------|---------|---------|

|    |         |     |    |         |         |         |         |         |         |
|----|---------|-----|----|---------|---------|---------|---------|---------|---------|
| 28 | 509-067 | D06 | 84 | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| 34 | 509-045 | EC7 | 90 | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| 5  | 509-058 | E05 | 88 | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 7 |  | 0.01486 | 0.00327 | 0.98187 | 0.70320 | 0.18921 | 0.10759 |
|---------|--|---------|---------|---------|---------|---------|---------|

|    |         |     |     |         |         |         |         |         |         |
|----|---------|-----|-----|---------|---------|---------|---------|---------|---------|
| 9  | 509-043 | H08 | 113 | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 11 | 509-061 | J04 | 65  | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| 7  | 509-078 | G09 | 107 | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 8 |  | 0.01486 | 0.00327 | 0.98187 | 0.70264 | 0.18963 | 0.10773 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.01523 | 0.00327 | 0.98150 | 0.70555 | 0.18804 | 0.10642 |
|            | STAND. DEV. | 0.00099 | 0.00001 | 0.00099 | 0.00640 | 0.00362 | 0.00279 |

# SECOND SUPERBATCH

|                     |       |       |       |        |        |        |
|---------------------|-------|-------|-------|--------|--------|--------|
| FUEL ELEMENT IDENT. | U-235 | U-236 | U-238 | PU-239 | PU-240 | PU 241 |
|---------------------|-------|-------|-------|--------|--------|--------|

|    |         |     |    |         |         |         |         |         |         |
|----|---------|-----|----|---------|---------|---------|---------|---------|---------|
| 40 | 509-041 | J08 | 60 | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
| 3  | 509-117 | J09 | 59 | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |
| 37 | 509-115 | C09 | 46 | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 1 |  | 0.01864 | 0.00361 | 0.97774 | 0.71731 | 0.17537 | 0.10732 |
|---------|--|---------|---------|---------|---------|---------|---------|

|    |         |     |    |         |         |         |         |         |         |
|----|---------|-----|----|---------|---------|---------|---------|---------|---------|
| 29 | 509-116 | J03 | 66 | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 2  | 509-111 | D10 | 49 | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| 36 | 509-118 | C04 | 79 | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 2 |  | 0.02113 | 0.00368 | 0.97519 | 0.73247 | 0.16605 | 0.10149 |
|---------|--|---------|---------|---------|---------|---------|---------|

|    |         |     |    |         |         |         |         |         |         |
|----|---------|-----|----|---------|---------|---------|---------|---------|---------|
| 30 | 509-112 | I03 | 69 | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 38 | 509-113 | I10 | 56 | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
| 31 | 509-114 | D03 | 76 | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 3 |  | 0.02111 | 0.00368 | 0.97521 | 0.73208 | 0.16624 | 0.10168 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.02029 | 0.00366 | 0.97605 | 0.72728 | 0.16922 | 0.10350 |
|            | STAND. DEV. | 0.00143 | 0.00004 | 0.00147 | 0.00864 | 0.00533 | 0.00331 |

CMC GENEIZATION ACCORDING ISOTOPE \*\*\* U-238 \*\*\*

ELEMENTS ORDERED ACCORDING INCREASING CONCENTRATION OF THE SELECTED ISOTOPE U-238

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1*509-109 F10 100   | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
| 2*509-116 J03 66    | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 3*509-112 I03 69    | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 4*509-114 D03 76    | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |
| 5*509-118 C04 79    | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |
| 6*509-115 C09 46    | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |
| 7*509-111 D10 49    | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| 8*509-113 I10 56    | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
| 9*509-117 J09 59    | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |
| 10*509-057 I05 115  | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |
| 11*509-053 E03 75   | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |
| 12*509-051 H10 55   | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| 13*509-052 I07 117  | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| 14*509-054 D08 86   | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| 15*509-074 F04 109  | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| 16*509-067 D06 84   | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| 17*509-043 H08 113  | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 18*509-058 E05 88   | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| 19*509-078 G09 107  | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
| 20*509-046 G05 103  | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| 21*509-055 H06 111  | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 22*509-076 F04 94   | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| 23*509-065 C07 82   | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| 24*509-059 I04 68   | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 25*509-073 J06 119  | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| 26*509-061 J04 65   | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| 27*509-045 E07 90   | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| 28*509-050 E09 92   | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| 29*509-075 F08 98   | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| 30*509-069 D04 78   | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |
| 31*509-044 I09 58   | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
| 32*509-048 C08 45   | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
| 33*509-071 G07 105  | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |
| 34*509-072 F06 96   | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
| 35*509-063 C05 80   | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
| 36*509-064 G10 108  | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
| 37*509-062 E10 50   | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |
| 38*509-042 H03 70   | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
| 39*509-047 F03 93   | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |
| 40*509-041 J08 60   | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |

# LIST OF REJECTED ELEMENTS

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1 509-073 J06 119   | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| 2 509-061 J04 65    | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| 3 509-045 E07 90    | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| 4 509-050 F09 92    | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| 5 509-075 F08 98    | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| 6 509-069 D04 78    | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |
| 7 509-044 I09 58    | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |

## FIRST SUPERBATCH

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1*509-109 F10 100   | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
| 10 509-059 I04 68   | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 28 509-067 D06 84   | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| BATCH 1             | 0.01756 | 0.00329 | 0.97915 | 0.71997 | 0.17947 | 0.10056 |
| 30*509-112 I03 69   | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 4 509-076 F04 94    | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| 6 509-074 H04 109   | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| BATCH 2             | 0.01712 | 0.00338 | 0.97951 | 0.71470 | 0.18125 | 0.10405 |
| 29*509-116 J03 66   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 35 509-065 C07 82   | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| 12 509-054 D08 86   | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| BATCH 3             | 0.01715 | 0.00337 | 0.97948 | 0.71532 | 0.18091 | 0.10377 |
| 31*509-114 D03 76   | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |
| 20 509-055 H06 111  | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 8 509-052 I07 117   | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| BATCH 4             | 0.01711 | 0.00338 | 0.97951 | 0.71469 | 0.18110 | 0.10421 |
| 36*509-118 C04 79   | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |
| 32 509-046 G05 103  | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| 25 509-051 H10 55   | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| BATCH 5             | 0.01716 | 0.00337 | 0.97947 | 0.71537 | 0.18088 | 0.10375 |
| 37*509-115 C09 46   | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |
| 7 509-078 G09 107   | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
| 27 509-053 E03 75   | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 6 |  | 0.01717 | 0.00337 | 0.97946 | 0.71565 | 0.18083 | 0.10351 |
|---------|--|---------|---------|---------|---------|---------|---------|

|                    |         |         |         |         |         |         |
|--------------------|---------|---------|---------|---------|---------|---------|
| 38*509-113 I10 56  | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
| 9 509-043 H08 113  | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 26 509-057 I05 115 | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 7 |  | 0.01726 | 0.00335 | 0.97939 | 0.71683 | 0.18045 | 0.10271 |
|---------|--|---------|---------|---------|---------|---------|---------|

|                  |         |         |         |         |         |         |
|------------------|---------|---------|---------|---------|---------|---------|
| 2*509-111 D10 49 | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| 5 509-058 E05 88 | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| 3*509-117 J09 59 | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 8 |  | 0.01893 | 0.00356 | 0.97751 | 0.72139 | 0.17413 | 0.10448 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.01743 | 0.00338 | 0.97918 | 0.71674 | 0.17988 | 0.10338 |
|            | STAND. DEV. | 0.00062 | 0.00008 | 0.00069 | 0.00255 | 0.00239 | 0.00126 |

# SECOND SUPERBATCH

|                     |       |       |       |        |        |        |
|---------------------|-------|-------|-------|--------|--------|--------|
| FUEL ELEMENT IDENT. | U-235 | U-236 | U-238 | PU-239 | PU-240 | PU 241 |
|---------------------|-------|-------|-------|--------|--------|--------|

|                   |         |         |         |         |         |         |
|-------------------|---------|---------|---------|---------|---------|---------|
| 21 509-072 F06 96 | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
| 33 509-042 H03 70 | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
| 22 509-062 E10 50 | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 1 |  | 0.01425 | 0.00338 | 0.98237 | 0.69512 | 0.19162 | 0.11326 |
|---------|--|---------|---------|---------|---------|---------|---------|

|                    |         |         |         |         |         |         |
|--------------------|---------|---------|---------|---------|---------|---------|
| 24 509-071 G07 105 | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |
| 18 509-047 F03 93  | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |
| 15 509-064 G10 108 | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 2 |  | 0.01424 | 0.00338 | 0.98238 | 0.69447 | 0.19201 | 0.11352 |
|---------|--|---------|---------|---------|---------|---------|---------|

|                   |         |         |         |         |         |         |
|-------------------|---------|---------|---------|---------|---------|---------|
| 14 509-048 C08 45 | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
| 40 509-041 J08 60 | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
| 17 509-063 C05 80 | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 3 |  | 0.01423 | 0.00338 | 0.98238 | 0.69448 | 0.19183 | 0.11369 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.01424 | 0.00338 | 0.98238 | 0.69469 | 0.19182 | 0.11349 |
|            | STAND. DEV. | 0.00001 | 0.00000 | 0.00001 | 0.00037 | 0.00020 | 0.00022 |



CMC GENIEZATION ACCORDING ISOTOPE \*\*\* PU-239 \*\*\*

ELEMENTS ORDERED ACCORDING INCREASING CONCENTRATION OF THE SELECTED ISOTOPE PU-239

| FUEL ELEMENT IDENT.  | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|----------------------|---------|---------|---------|---------|---------|---------|
| 1. 509-041 J08. 60   | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
| 2. 509-047 F03. 93   | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |
| 3. 509-064 G10. 108  | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
| 4. 509-042 H03. 70   | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
| 5. 509-062 E10. 50   | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |
| 6. 509-063 C05. 80   | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
| 7. 509-048 C08. 45   | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
| 8. 509-044 I09. 58   | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
| 9. 509-072 F06. 96   | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
| 10. 509-071 G07. 125 | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |
| 11. 509-069 D04. 78  | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |
| 12. 509-075 F08. 98  | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| 13. 509-050 F09. 92  | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| 14. 509-061 J04. 65  | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| 15. 509-045 E07. 90  | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| 16. 509-073 J06. 119 | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| 17. 509-065 C07. 82  | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| 18. 509-059 I04. 68  | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 19. 509-076 F04. 94  | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| 20. 509-046 G05. 103 | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| 21. 509-078 G09. 107 | 0.01495 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
| 22. 509-055 H06. 111 | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 23. 509-043 H08. 113 | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 24. 509-058 E05. 88  | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| 25. 509-067 D06. 84  | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| 26. 509-074 H04. 109 | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| 27. 509-054 D08. 86  | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| 28. 509-052 I07. 117 | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| 29. 509-051 H10. 55  | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| 30. 509-053 E03. 75  | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |
| 31. 509-057 I05. 115 | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |
| 32. 509-117 J09. 59  | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |
| 33. 509-113 I10. 56  | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
| 34. 509-111 D10. 49  | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| 35. 509-118 C04. 79  | 0.02103 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |
| 36. 509-119 C09. 46  | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |
| 37. 509-114 C03. 76  | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |
| 38. 509-112 I03. 69  | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 39. 509-116 J03. 66  | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 40. 509-109 F10. 100 | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |

# LIST OF REJECTED ELEMENTS

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1 509-067 D06 84    | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| 2 509-074 H04 109   | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| 3 509-054 D08 86    | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| 4 509-052 I07 117   | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| 5 509-051 H10 55    | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| 6 509-053 E03 75    | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |
| 7 509-057 I05 115   | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |

## FIRST SUPERBATCH

| FUEL ELEMENT IDENT.  | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|----------------------|---------|---------|---------|---------|---------|---------|
| 40. 509-041 J08. 60  | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
| 5 509-058 E05 88     | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| 16 509-073 J06 119   | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| BATCH 1              | 0.01460 | 0.00332 | 0.98208 | 0.69913 | 0.19049 | 0.11038 |
| 18 509-047 F03 93    | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |
| 9 509-043 H08 113    | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 34 509-045 E07 90    | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| BATCH 2              | 0.01457 | 0.00332 | 0.98211 | 0.69891 | 0.19065 | 0.11044 |
| 15 509-064 G10 108   | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
| 20 509-055 H06 111   | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 11 509-061 J04 65    | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| BATCH 3              | 0.01459 | 0.00332 | 0.98209 | 0.69908 | 0.19067 | 0.11025 |
| 33 509-042 H03 70    | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
| 7 509-078 G09 107    | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
| 19 509-050 E09 92    | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| BATCH 4              | 0.01455 | 0.00332 | 0.98212 | 0.69885 | 0.19070 | 0.11045 |
| 17 509-063 C05 80    | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
| 4 509-076 F04 94     | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| 23 509-075 F08 98    | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| BATCH 5              | 0.01454 | 0.00333 | 0.98213 | 0.69875 | 0.19062 | 0.11063 |
| 13 509-044 I09 58    | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
| 35 509-065 C07 82    | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| 39. 509-069. D04. 78 | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 6 |  | 0.01452 | 0.00333 | 0.98215 | 0.69857 | 0.19057 | 0.11086 |
|---------|--|---------|---------|---------|---------|---------|---------|

|    |         |     |     |         |         |         |         |         |         |
|----|---------|-----|-----|---------|---------|---------|---------|---------|---------|
| 22 | 509-062 | E10 | 50  | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |
| 32 | 509-046 | G05 | 103 | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| 24 | 509-071 | G07 | 105 | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 7 |  | 0.01452 | 0.00333 | 0.98215 | 0.69855 | 0.19061 | 0.11084 |
|---------|--|---------|---------|---------|---------|---------|---------|

|    |         |     |    |         |         |         |         |         |         |
|----|---------|-----|----|---------|---------|---------|---------|---------|---------|
| 14 | 509-048 | C08 | 45 | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
| 10 | 509-059 | I04 | 68 | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 21 | 509-072 | F06 | 56 | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 8 |  | 0.01450 | 0.00333 | 0.98217 | 0.69858 | 0.19065 | 0.11078 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.01455 | 0.00333 | 0.98212 | 0.69880 | 0.19062 | 0.11058 |
|            | STAND. DEV. | 0.00004 | 0.00001 | 0.00003 | 0.00023 | 0.00007 | 0.00023 |

# SECOND SUPERBATCH

| FUEL ELEMENT IDENT. |  | U-235 | U-236 | U-238 | PU-239 | PU-240 | PU 241 |
|---------------------|--|-------|-------|-------|--------|--------|--------|
|---------------------|--|-------|-------|-------|--------|--------|--------|

|            |     |    |         |         |         |         |         |         |
|------------|-----|----|---------|---------|---------|---------|---------|---------|
| 2*509-111  | D10 | 49 | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| 36*509-112 | I03 | 69 | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 31*509-114 | D03 | 76 | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 1 |  | 0.02111 | 0.00368 | 0.97521 | 0.73220 | 0.16612 | 0.10168 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |     |    |         |         |         |         |         |         |
|------------|-----|----|---------|---------|---------|---------|---------|---------|
| 38*509-113 | I10 | 56 | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
| 29*509-116 | J03 | 66 | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 37*509-115 | C09 | 46 | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 2 |  | 0.02112 | 0.00368 | 0.97520 | 0.73235 | 0.16612 | 0.10153 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |     |     |         |         |         |         |         |         |
|------------|-----|-----|---------|---------|---------|---------|---------|---------|
| 3*509-117  | J09 | 59  | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |
| 1*509-109  | F10 | 103 | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
| 36*509-118 | C04 | 79  | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 3 |  | 0.02158 | 0.00359 | 0.97483 | 0.73734 | 0.16468 | 0.09798 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.02127 | 0.00365 | 0.97508 | 0.73396 | 0.16564 | 0.10040 |
|            | STAND. DEV. | 0.00027 | 0.00005 | 0.00022 | 0.00293 | 0.00083 | 0.00209 |

CMOGENEIZATION ACCORDING ISOTOPE \*\*\* PU-240 \*\*\*

ELEMENTS ORDERED ACCORDING ENCREASING CONCENTRATION OF THE SELECTED ISOTOPE PU-240

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1*509-109 F10 100   | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
| 2*509-116 J03 66    | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 3*509-112 I03 69    | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 4*509-115 C09 46    | 0.02102 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |
| 5*509-114 D03 76    | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |
| 6*509-118 C04 79    | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |
| 7*509-111 C10 49    | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| 8*509-112 I10 56    | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
| 9*509-117 J09 59    | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |
| 10 509-057 I05 115  | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |
| 11 509-053 E03 75   | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |
| 12 509-051 H10 55   | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| 13 509-054 D08 86   | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| 14 509-052 I07 117  | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| 15 509-058 E05 88   | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| 16 509-074 H04 109  | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| 17 509-067 D06 84   | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| 18 509-043 H08 113  | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 19 509-055 F06 111  | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 20 509-046 G05 103  | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| 21 509-078 G09 107  | 0.01495 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
| 22 509-059 I04 68   | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 23 509-076 F04 94   | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| 24 509-065 C07 82   | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| 25 509-073 J06 119  | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| 26 509-045 E07 90   | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| 27 509-061 J04 65   | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| 28 509-075 F08 98   | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| 29 509-050 E09 92   | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| 30 509-069 D04 78   | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |
| 31 509-071 G07 105  | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |
| 32 509-044 I09 58   | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
| 33 509-072 F06 96   | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
| 34 509-063 C05 80   | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
| 35 509-048 C08 45   | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
| 36 509-062 E10 50   | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |
| 37 509-042 F03 70   | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
| 38 509-064 G10 108  | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
| 39 509-041 J08 60   | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
| 40 509-047 F03 93   | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |

# LIST OF REJECTED ELEMENTS

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1 509-072 J06 119   | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| 2 509-045 F07 90    | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| 3 509-061 J04 65    | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| 4 509-075 F08 98    | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| 5 509-050 F09 92    | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| 6 509-065 D04 78    | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |
| 7 509-071 G07 105   | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |

## FIRST SUPERBATCH

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1*509-109 F10 100   | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.06789 |
| 35 509-065 C07 82   | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10600 |
| 6 509-074 F04 109   | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| BATCH 1             | 0.01759 | 0.00328 | 0.97912 | 0.72015 | 0.17958 | 0.10027 |
| 30*509-112 I03 69   | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 10 509-059 I04 68   | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 5 509-058 E05 88    | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| BATCH 2             | 0.01703 | 0.00339 | 0.97957 | 0.71408 | 0.18113 | 0.10479 |
| 29*509-116 J03 66   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 4 509-076 F04 94    | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| 8 509-052 I07 117   | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| BATCH 3             | 0.01720 | 0.00336 | 0.97944 | 0.71560 | 0.18091 | 0.10349 |
| 2*509-111 C10 49    | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| 9 509-043 H08 113   | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
| 12 509-054 D08 86   | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| BATCH 4             | 0.01707 | 0.00339 | 0.97955 | 0.71443 | 0.18108 | 0.10448 |
| 36*509-118 C04 79   | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |
| 20 509-055 H06 111  | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 25 509-051 H10 55   | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| BATCH 5             | 0.01716 | 0.00337 | 0.97947 | 0.71543 | 0.18085 | 0.10372 |
| 31*509-114 D03 76   | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |
| 32 509-046 G05 103  | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| 27 509-053 E03 75   | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 6 |  | 0.01718 | 0.00337 | 0.97945 | 0.71568 | 0.18080 | 0.10352 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |     |     |         |         |         |         |         |         |
|------------|-----|-----|---------|---------|---------|---------|---------|---------|
| 38*509-113 | I10 | 56  | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |
| 28 509-067 | D06 | 84  | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| 26 509-057 | I05 | 115 | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 7 |  | 0.01727 | 0.00335 | 0.97938 | 0.71703 | 0.18039 | 0.10258 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |     |     |         |         |         |         |         |         |
|------------|-----|-----|---------|---------|---------|---------|---------|---------|
| 37*509-115 | C09 | 46  | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |
| 7 509-078  | G09 | 107 | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
| 3*509-117  | J09 | 59  | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 8 |  | 0.01896 | 0.00356 | 0.97748 | 0.72152 | 0.17428 | 0.10421 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.01743 | 0.00338 | 0.97918 | 0.71674 | 0.17988 | 0.10338 |
|            | STAND. DEV. | 0.00064 | 0.00008 | 0.00070 | 0.00270 | 0.00232 | 0.00143 |

# SECOND SUPERBATCH

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 21 509-072 F06 96   | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
| 40 509-041 J08 60   | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
| 33 509-042 F03 70   | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 1 |  | 0.01419 | 0.00339 | 0.98242 | 0.69415 | 0.19188 | 0.11397 |
|---------|--|---------|---------|---------|---------|---------|---------|

|                    |         |         |         |         |         |         |
|--------------------|---------|---------|---------|---------|---------|---------|
| 17 509-063 C05 80  | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
| 15 509-064 G10 108 | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
| 22 509-062 E10 50  | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 2 |  | 0.01425 | 0.00338 | 0.98237 | 0.69468 | 0.19183 | 0.11349 |
|---------|--|---------|---------|---------|---------|---------|---------|

|                   |         |         |         |         |         |         |
|-------------------|---------|---------|---------|---------|---------|---------|
| 13 509-044 I09 58 | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
| 18 509-047 F03 93 | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |
| 14 509-048 C08 45 | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |

|         |  |         |         |         |         |         |         |
|---------|--|---------|---------|---------|---------|---------|---------|
| BATCH 3 |  | 0.01428 | 0.00337 | 0.98234 | 0.69505 | 0.19178 | 0.11317 |
|---------|--|---------|---------|---------|---------|---------|---------|

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.01424 | 0.00338 | 0.98238 | 0.69463 | 0.19183 | 0.11354 |
|            | STAND. DEV. | 0.00004 | 0.00001 | 0.00004 | 0.00045 | 0.00005 | 0.00040 |

CMC GENEIZATION ACCORDING ISOTOPE \*\*\* PU 241 \*\*\*

ELEMENTS ORDERED ACCORDING INCREASING CONCENTRATION OF THE SELECTED ISOTOPE PU 241

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1*559-109 FI 100    | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
| 2*559-109 FI 100    | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
| 3*559-116 J03 66    | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 4*559-112 J03 69    | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 5*559-112 J03 69    | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 6*559-114 D03 76    | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 7*559-118 C04 79    | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 8*559-115 C09 46    | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 9*559-111 H10 55    | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 10*559-111 D10 49   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 11*559-113 I10 56   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 12*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 13*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 14*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 15*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 16*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 17*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 18*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 19*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 20*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 21*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 22*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 23*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 24*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 25*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 26*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 27*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 28*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 29*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 30*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 31*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 32*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 33*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 34*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 35*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 36*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 37*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 38*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 39*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 40*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 41*559-117 J09 59   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |



# LIST OF REJECTED ELEMENTS

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1 509-073 J06 119   | 0.01476 | 0.00329 | 0.98195 | 0.70096 | 0.19024 | 0.10880 |
| 2 509-045 E07 90    | 0.01454 | 0.00333 | 0.98213 | 0.69947 | 0.19029 | 0.11024 |
| 3 509-061 J04 65    | 0.01456 | 0.00332 | 0.98211 | 0.69893 | 0.19070 | 0.11037 |
| 4 509-050 E09 92    | 0.01447 | 0.00334 | 0.98219 | 0.69808 | 0.19083 | 0.11109 |
| 5 509-075 F08 98    | 0.01440 | 0.00335 | 0.98225 | 0.69760 | 0.19077 | 0.11163 |
| 6 509-069 D04 78    | 0.01437 | 0.00336 | 0.98227 | 0.69704 | 0.19091 | 0.11204 |
| 7 509-071 G07 105   | 0.01435 | 0.00336 | 0.98229 | 0.69695 | 0.19097 | 0.11208 |

## FIRST SUPERBATCH

| FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------------------|---------|---------|---------|---------|---------|---------|
| 1*509-109 F10 100   | 0.02282 | 0.00335 | 0.97383 | 0.75173 | 0.16038 | 0.08789 |
| 35 509-065 C07 82   | 0.01484 | 0.00327 | 0.98189 | 0.70230 | 0.18971 | 0.10800 |
| 28 509-067 D06 84   | 0.01506 | 0.00324 | 0.98170 | 0.70532 | 0.18870 | 0.10598 |
| BATCH 1             | 0.01757 | 0.00329 | 0.97914 | 0.71978 | 0.17960 | 0.10062 |
| 29*509-116 J03 66   | 0.02138 | 0.00363 | 0.97499 | 0.73555 | 0.16519 | 0.09927 |
| 4 509-076 F04 94    | 0.01492 | 0.00326 | 0.98182 | 0.70310 | 0.18968 | 0.10723 |
| 6 509-074 H04 109   | 0.01513 | 0.00322 | 0.98165 | 0.70644 | 0.18865 | 0.10491 |
| BATCH 2             | 0.01714 | 0.00337 | 0.97948 | 0.71503 | 0.18117 | 0.10380 |
| 26 509-057 I05 115  | 0.01581 | 0.00310 | 0.98109 | 0.71566 | 0.18559 | 0.09875 |
| 10 509-059 I04 68   | 0.01481 | 0.00328 | 0.98191 | 0.70286 | 0.18933 | 0.10781 |
| 12 509-054 D08 86   | 0.01523 | 0.00321 | 0.98157 | 0.70811 | 0.18783 | 0.10406 |
| BATCH 3             | 0.01528 | 0.00320 | 0.98152 | 0.70888 | 0.18758 | 0.10354 |
| 30*509-112 I03 69   | 0.02130 | 0.00364 | 0.97505 | 0.73458 | 0.16541 | 0.10001 |
| 32 509-046 G05 103  | 0.01498 | 0.00325 | 0.98177 | 0.70416 | 0.18909 | 0.10675 |
| 8 509-052 I07 117   | 0.01530 | 0.00319 | 0.98151 | 0.70816 | 0.18787 | 0.10397 |
| BATCH 4             | 0.01719 | 0.00336 | 0.97944 | 0.71563 | 0.18079 | 0.10357 |
| 27 509-053 E03 75   | 0.01550 | 0.00316 | 0.98135 | 0.71131 | 0.18688 | 0.10181 |
| 20 509-055 H06 111  | 0.01498 | 0.00325 | 0.98177 | 0.70435 | 0.18901 | 0.10664 |
| 3*509-117 J09 59    | 0.02085 | 0.00373 | 0.97542 | 0.72890 | 0.16721 | 0.10389 |
| BATCH 5             | 0.01711 | 0.00338 | 0.97951 | 0.71485 | 0.18104 | 0.10411 |
| 31*509-114 D03 76   | 0.02107 | 0.00369 | 0.97525 | 0.73156 | 0.16642 | 0.10202 |
| 5 509-058 E05 88    | 0.01499 | 0.00325 | 0.98176 | 0.70481 | 0.18865 | 0.10654 |
| 38*509-113 I10 56   | 0.02095 | 0.00371 | 0.97534 | 0.73010 | 0.16688 | 0.10303 |

|         |                   |         |         |         |         |         |         |
|---------|-------------------|---------|---------|---------|---------|---------|---------|
| BATCH 6 |                   | C.01900 | 0.00355 | 0.97745 | 0.72216 | 0.17398 | 0.10386 |
|         | 36*509-118 C04 79 | 0.02105 | 0.00369 | 0.97525 | 0.73140 | 0.16644 | 0.10216 |
|         | 7 509-078 G09 107 | 0.01499 | 0.00325 | 0.98176 | 0.70424 | 0.18931 | 0.10645 |
|         | 2*509-111 D10 49  | 0.02095 | 0.00371 | 0.97534 | 0.73045 | 0.16652 | 0.10303 |
| BATCH 7 |                   | 0.01900 | 0.00355 | 0.97745 | 0.72203 | 0.17409 | 0.10388 |
|         | 37*509-115 C09 46 | 0.02103 | 0.00369 | 0.97527 | 0.73140 | 0.16631 | 0.10228 |
|         | 9 509-043 H08 113 | 0.01503 | 0.00324 | 0.98173 | 0.70474 | 0.18890 | 0.10636 |
|         | 25 509-051 H10 55 | 0.01545 | 0.00317 | 0.98138 | 0.71054 | 0.18712 | 0.10234 |
| BATCH 8 |                   | 0.01717 | 0.00337 | 0.97946 | 0.71556 | 0.18078 | 0.10366 |

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.01743 | 0.00338 | 0.97918 | 0.71674 | 0.17588 | 0.10338 |
|            | STAND. DEV. | 0.00119 | 0.00012 | 0.00130 | 0.00443 | 0.00435 | 0.00113 |

# SECOND SUPERBATCH

|         | FUEL ELEMENT IDENT. | U-235   | U-236   | U-238   | PU-239  | PU-240  | PU 241  |
|---------|---------------------|---------|---------|---------|---------|---------|---------|
|         | 13 509-044 I09 58   | 0.01436 | 0.00336 | 0.98228 | 0.69637 | 0.19108 | 0.11255 |
|         | 33 509-042 H03 70   | 0.01421 | 0.00339 | 0.98241 | 0.69424 | 0.19195 | 0.11381 |
|         | 15 509-064 G10 108  | 0.01423 | 0.00338 | 0.98239 | 0.69395 | 0.19231 | 0.11374 |
| BATCH 1 |                     | 0.01427 | 0.00338 | 0.98236 | 0.69485 | 0.19178 | 0.11337 |
|         | 21 509-072 F06 96   | 0.01434 | 0.00336 | 0.98230 | 0.69660 | 0.19112 | 0.11228 |
|         | 18 509-047 F03 93   | 0.01414 | 0.00340 | 0.98247 | 0.69251 | 0.19276 | 0.11473 |
|         | 22 509-062 E10 50   | 0.01422 | 0.00338 | 0.98240 | 0.69453 | 0.19178 | 0.11368 |
| BATCH 2 |                     | 0.01423 | 0.00338 | 0.98239 | 0.69455 | 0.19189 | 0.11357 |
|         | 14 509-048 C08 45   | 0.01435 | 0.00336 | 0.98229 | 0.69628 | 0.19149 | 0.11223 |
|         | 40 509-041 J08 60   | 0.01404 | 0.00342 | 0.98254 | 0.69162 | 0.19258 | 0.11580 |
|         | 17 509-063 C05 80   | 0.01431 | 0.00337 | 0.98232 | 0.69555 | 0.19141 | 0.11304 |
| BATCH 3 |                     | 0.01423 | 0.00338 | 0.98238 | 0.69448 | 0.19183 | 0.11369 |

|            |             |         |         |         |         |         |         |
|------------|-------------|---------|---------|---------|---------|---------|---------|
| SUPERBATCH | MEAN VALUES | 0.01424 | 0.00338 | 0.98238 | 0.69463 | 0.19183 | 0.11354 |
|            | STAND. DEV. | 0.00002 | 0.00000 | 0.00002 | 0.00020 | 0.00005 | 0.00016 |



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0037 232 FORMAT (/)
0038 233 FORMAT (1H ,8X,'H(' ,I2,') =' ,F9.2)
0039 234 FORMAT(////)
0040 235 FORMAT (////////,' PART OF THE INVENTORY CONTAINED IN EACH OUTPUT BATCH'
0041 1CH',//)
0041 236 FORMAT (////////,' CONFIDENCE INTERVALS',///,
0042 1' P(X) X-MEAN X',//)
0042 237 FORMAT (15,F8.1,2F12.2)
0043 238 FORMAT (///,' FOR INCOMPATIBILITY AMONG PROGRAM DIMENSIONS,QMS AND
0043 1 DM, THE VALUE OF QMS HAS BEEN REDUCED TO',F6.2,///)

C
0044 301 FORMAT (5I10)
0045 302 FORMAT (5F12.7)
0046 303 FORMAT (5F10.2)

C
C ***** ***** ***** *****
C
0047 REAL STAR/'*'/
0048 DIMENSION STARS(100)
0049 DO 501 J=1,100
0050 STARS(J)=STAR
0051 501 CONTINUE

C
0052 WRITE (6,200)
0053 READ (5,110) SCRITT
0054 WRITE (6,230) SCRITT
0055 WRITE (6,234)

C
0056 DO 5 J=1,2
0057 READ (5,110) SCRITT
0058 WRITE (6,230) SCRITT
0059 WRITE (6,232)
0060 READ (5,110) SCRITT
0061 WRITE (6,230) SCRITT
0062 WRITE (6,231)
0063 READ (5,101) NB(J)
0064 NBB=NB(J)
0065 DO 1 K=1,NBB
0066 READ (5,104) T(J,K),XX(J,K)
0067 1 CONTINUE
0068 A1=0.
0069 A3=0.
0070 NBB=NB(J)
0071 DO 2 K=1,NBB
0072 A1=A1+T(J,K)*XX(J,K)
0073 A3=A3+T(J,K)
0074 2 CONTINUE
0075 DO 4 K=1,NBB

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0076 P(J,K)=T(J,K)/A3
0077 4 CONTINUE
0078 XC(J)=A1/A3
0079 WRITE (6,212) ((K,T(J,K),XX(J,K), P(J,K)),K=1,NBB)
0080 WRITE (6,232)
0081 READ (5,110) SCRITT
0082 WRITE (6,230) SCRITT
0083 WRITE (6,231)
0084 WRITE (6,208) (J,NB(J),XC(J))
0085 WRITE (6,234)
0086 5 CCNTINUE
0087 C1=XC(1)
0088 C2=XC(2)
0089 C
0090 WRITE (6,200)
0091 READ (5,110) SCRITT
0092 WRITE (6,230) SCRITT
0093 WRITE (6,234)
0094 READ (5,101) NBATCH
0095 READ (5,110) SCRITT
0096 WRITE (6,230) SCRITT
0097 WRITE (6,231)
0098 READ (5,103) ((M(J),SM(J),X(J),SX(J)),J=1,NBATCH)
0099 DO 9 J=1,NBATCH
0100 WRITE (6,205) (J,M(J),SM(J),X(J),SX(J))
0101 9 CONTINUE
0102 C
0103 MM=0.
0104 DC=C1-C2
0105 DO 14 K=1,NBATCH
0106 HH(K)=M(K)*(X(K)-C2)/DC
0107 MM=MM+HH(K)
0108 14 CONTINUE
0109 WRITE (6,235)
0110 WRITE (6,233) ((K,HH(K)),K=1,NBATCH)
0111 WRITE (6,209) MM
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0119 WRITE (6,201) IX,RND
0120 WRITE (6,202) NPROVE
0121 C=100./FLOAT(NPROVE)
0122 READ (5,101) NCL
0123 READ (5,102) (CL(J),J=1,NCL)
0124 READ (5,101) IFUNCH
C
0125 DO 71 LG=1,62
0126 71 LD(LG)=0.
0127 Q1=0.
0128 Q2=0.
C
0129 LX=INT(QMS/DM)
0130 IF (LX.LT.30) GO TO 50
0131 QMS=30*DM
0132 LMX=62
0133 WRITE (6,238) CMS
0134 GO TO 52
0135 50 CONTINUE
0136 AMM=MM-QMS
0137 IF (AMOD(QMS,DM).LT.(DM*.01)) GO TO 51
0138 LX=LX+1
0139 QMS=LX*DM
0140 51 CONTINUE
0141 LMX=2*LX+2
0142 52 CONTINUE
C
0143 Q(1)=MM-DM*(FLCAT(LX)+0.5)
0144 DO 55 J=2,LMX
0145 Q(J)=Q(1)+(J-1)*DM
0146 55 CONTINUE
C
0147 DO 13 L=1,NPROVE
0148 DO 31 J=1,2
0149 A1=0.
0150 A3=0.
0151 NBB=NB(J)
0152 DO 32 K=1,NBB
0153 A4=RANDOM(0.)*T(J,K)
0154 A1=A1+XX(J,K)*A4
0155 A3=A3+A4
0156 32 CONTINUE
0157 EXJ(J)=A1/A3
0158 31 CONTINUE
0159 EC1=EXJ(1)
0160 EC2=EXJ(2)
0161 DD=EC1-EC2
0162 DO 11 K=1,NBATCH

```

```

0163 417 CALL GAUSS(IX,SM(K),M(K),EM(K))
0164 418 CALL GAUSS(IX, SX(K),X(K),EX(K))
0165 11 CONTINUE
0166 EQQ=0.
0167 DO 12 K=1,NBATCH
0168 EQQ=EQQ+EM(K)*(EX(K)-EC2)/DD
0169 12 CONTINUE
C
0170 Q1=Q1+EQQ
0171 Q2=Q2+EQQ*EQQ
0172 LG=(EQQ-AMM)/DM+2
0173 IF (LG.LT.1) LG=1
0174 IF (LG.GT.LMX) LG=LMX
0175 LD(LG)=LD(LG)+1
0176 13 CONTINUE
C
0177 VMED=Q1/NPROVE
0178 VAR=Q2/NPROVE-VMED*VMED
0179 SDEV=SQRT(VAR)
0180 PERC=(SDEV/VMED)*100.
0181 WRITE (6,226) DM
0182 LMX1=LMX-1
0183 WRITE (6,227) LD(LG),LG=1,LMX)
0184 I=LD(1)
0185 DO 15 J=2,LMX
0186 K=LD(J)
0187 I=MAX0(I,K)
0188 15 CONTINUE
0189 DO 16 J=2,LMX1
0190 K7(J)=LD(J)*50/I
0191 16 CONTINUE
C
0192 DO 520 J=1,LMX
0193 PDF(J)=FLOAT(LD(J))/PROVE
0194 520 CONTINUE
0195 IF (IPUNCH.NE.777) GC TO 521
0196 IN=1
0197 DO 60 J=1,LMX
0198 IF (PDF(J).NE.0.) GO TO 61
0199 IN=IN+1
0200 60 CONTINUE
0201 61 CONTINUE
0202 IL=LMX
0203 DO 62 J=1,LMX
0204 K=LMX-J+1
0205 IF (PDF(K).NE.0.) GC TO 63
0206 IL=IL-1
0207 62 CONTINUE

```



```

0208 63 CONTINUE
0209 LU=IL-IN+1
0210 WRITE (7,301) LU
0211 WRITE (7,303) (Q(IN),VMED,SDEV)
0212 WRITE (7,302) (PDF(J),J=IN,IL)
0213 521 CONTINUE
C
0214 WRITE (6,234)
0215 WRITE (6,222)
0216 DO 500 JJ=2,LMX1
0217 LLL=K7(JJ)
0218 IF (LLL.LE.0) GO TO 499
0219 WRITE (6,228) (Q(JJ),PDF(JJ),(STARS(J),J=1,LLL))
0220 GO TO 500
0221 499 CONTINUE
0222 WRITE (6,225) (Q(JJ),PDF(JJ))
0223 500 CONTINUE
C
0224 I=1
0225 CCC=CL(I)
0226 NUM(1)=LD(1)
0227 ANUM(1)=NUM(1)*C
0228 DO 513 J=2,LMX
0229 J1=J-1
0230 NUM(J)=NUM(J1)+LD(J)
0231 ANUM(J)=NUM(J)*C
0232 IF (I.GT.NCL) GO TO 57
0233 IF (ANUM(J).LT.CCC) GO TO 57
0234 QL(I)=Q(J)-DM*(ANUM(J)-CCC)/(ANUM(J)-ANUM(J-1))
0235 I=I+1
0236 CCC=CL(I)
0237 57 CONTINUE
0238 512 CONTINUE
C
0239 WRITE (6,200)
0240 WRITE (6,227) (NUM(J),J=1,LMX)
0241 WRITE (6,234)
C
0242 WRITE (6,223)
0243 DO 511 J=2,LMX
0244 PDF(J)=PDF(J-1)+PDF(J)
0245 511 CONTINUE
C
0246 UM=NUM(LMX)
0247 F=1000/UM
0248 DO 514 LG=1,LMX
0249 LD(LG)=NUM(LG)*F
0250 514 CONTINUE

```

```

0251 DO 515 JJ=1,LMX
0252 LLL=LD(JJ)
0253 IF (LLL.LE.0) GO TO 516
0254 WRITE (6,228) (Q(JJ),PDF(JJ),(STARS(J),J=1,LLL))
0255 GO TO 515
516 CONTINUE
0256 WRITE (6,225) (Q(JJ),PDF(JJ))
0257 CONTINUE
518 WRITE (6,203) VMED,SDEV,PERC,MM
0260 WRITE (6,236)
0261 DO 59 J=1,NCL
0262 QD=QL(J)-VMED
0263 WRITE (6,237) (J,CL(J),QD,QL(J))
0264 59 CONTINUE
0265 STOP
0266 END

```

```

0001 SUBROUTINE SETRND (JARG)
C
C
C INITIALIZE RANDOM SERIES
0002 INTEGER IARG/221/
0003 IF (JARG.NE.0) IARG=JARG
0004 IF (MOD(IARG,2).EQ.0) IARG=IARG+1
0005 RETURN
C
C
C ENTRY RANDOM (DUM)
0006 PRODUCE A RANDOM NUMBER UNIFORMLY DISTRIBUTE BETWEEN
1 AND 0
C
C
C IARG=IARG*65539
0007 IF (IARG) 5,6,6
0008 5 IARG=IARG+2147483647+1
0009 6 RANDOM=IARG*0.4656613E-9
0010 RETURN
C
C
C ENTRY STLAST (LAST)
0012 STORE IN 'LAST' THE LAST VALUE OF IARG.
C
C
C LAST=IARG
0013 RETURN
0014 END
0015

```



SUBROUTINE RANDU

## PURPOSE

COMPUTES UNIFORMLY DISTRIBUTED RANDOM REAL NUMBERS BETWEEN 0 AND 1.0 AND RANDOM INTEGERS BETWEEN ZERO AND 2\*\*31. EACH ENTRY USES AS INPUT AN INTEGER RANDOM NUMBER AND PRODUCES A NEW INTEGER AND REAL RANDOM NUMBER.

## USAGE

```
CALL RANDU(IX,IY,YFL)
```

## DESCRIPTION OF PARAMETERS

IX - FOR THE FIRST ENTRY THIS MUST CONTAIN ANY ODD INTEGER NUMBER WITH NINE OR LESS DIGITS. AFTER THE FIRST ENTRY, IX SHOULD BE THE PREVIOUS VALUE OF IY COMPUTED BY THIS SUBROUTINE.

IIY - A RESULTANT INTEGER RANDOM NUMBER REQUIRED FOR THE NEXT ENTRY TO THIS SUBROUTINE. THE RANGE OF THIS NUMBER IS BETWEEN ZERO AND 2\*\*31

YFL- THE RESULTANT UNIFORMLY DISTRIBUTED, FLOATING POINT,  
RANDOM NUMBER IN THE RANGE 0 TO 1.0

REMARKS

THIS SUBROUTINE IS SPECIFIC TO SYSTEM/360  
THIS SUBROUTINE WILL PRODUCE 2\*\*29 TERMS  
BEFORE REPEATING

SUBROUTINES AND FUNCTION SJBPROGRAMS REQUIRED  
NONE

## METHOD

POWER RESIDUE METHOD DISCUSSED IN IBM MANUAL C20-8011,  
RANDOM NUMBER GENERATION AND TESTING

SUBROUTINE RANDU(IX,IY,YFL)

IY=IX\*65539

IF(IY)5,6,6

5  $IY = IY + 2147483647 + 1$

6  $\underline{YFL=IY}$

$$YFL=YFL*.4656613E-9$$

## RETURN

END

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0008

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 RANDU0045  
 RANDU0046

\*\*\* LIST OF THE DATA CARDS USED FOR THE 'CC2' SAMPLE PROGRAM

\*\*\* INPUT BATCH DATA \*\*\*

REACTOR CANDU  
BATCH TOTAL PU (G) PU-241 PERC WEIGHT FACTOR

3434.4 3.41  
3218.4 3.67  
3301.0 3.61  
3306.7 3.72

REACTOR BATCH NUMB. MEAN PERC.T CONCENT.N

REACTOR VAK  
BATCH TOTAL PU (G) PU-241 PERC WEIGHT FACTOR

3103.5 7.53  
2109.6 8.06  
4308.0 8.10  
702.7 7.74

REACTOR BATCH NUMB. MEAN PERC.T CONCENT.N

\*\*\* OUTPUT BATCH DATA \*\*\*

| N      | MASS    | MASS-SD | PU/241   | PU/241-SD |
|--------|---------|---------|----------|-----------|
| 2881.1 | 14.4055 | 5.556   | 0.027980 |           |
| 2350.7 | 11.7535 | 6.519   | 0.032595 |           |
| 2657.0 | 13.2850 | 7.472   | 0.037360 |           |
| 3736.0 | 18.9300 | 7.667   | 0.036335 |           |

\*\*\* STATISTICAL ANALYSIS INPUT DATA \*\*\*

375

10000

1200 50.

2.5 8

90. 55. 5.0

000

10. 57.5

20.

80.

NPRCVE

WITHOUT PUNCHED CARDS

\*\* INPUT BATCH DATA \*\*

REACTOR CANDU

| BATCH | TOTAL PU (G) | PU-241 PERC | WEIGHT FACTOR |
|-------|--------------|-------------|---------------|
| 1     | 3434.3999    | 3.4100      | 0.2559        |
| 2     | 3218.3999    | 3.6700      | 0.2398        |
| 3     | 3381.0000    | 3.8100      | 0.2519        |
| 4     | 3386.7000    | 3.7200      | 0.2524        |

| REACTOR | BATCH NUMB. | MEAN PERC. T CONCENT. N |
|---------|-------------|-------------------------|
| 1       | 4           | 3.6514                  |

REACTOR VAK

| BATCH | TOTAL PU (G) | PU-241 PERC | WEIGHT FACTOR |
|-------|--------------|-------------|---------------|
| 1     | 3103.5000    | 7.5300      | 0.3035        |
| 2     | 2109.5999    | 8.6800      | 0.2063        |
| 3     | 4309.0000    | 8.1800      | 0.4214        |
| 4     | 702.7000     | 7.7400      | 0.0667        |

| REACTOR | BATCH NUMB. | MEAN PERC. T CONCENT. N |
|---------|-------------|-------------------------|
| 2       | 4           | 7.9318                  |

**\*\* OUTPUT BATCH DATA \*\***

| N | MASS      | MASS-SD | PU/241 | PU/241-SD |
|---|-----------|---------|--------|-----------|
| 1 | 2881.0999 | 14.4055 | 5.5960 | 0.0280    |
| 2 | 2350.7000 | 11.7535 | 6.5190 | 0.0326    |
| 3 | 2657.0000 | 13.2850 | 7.4720 | 0.0374    |
| 4 | 3786.0000 | 18.9300 | 7.6670 | 0.0383    |

**PART OF THE INVENTORY CONTAINED IN EACH OUTPUT BATCH**

|         |         |
|---------|---------|
| H( 1) = | 1572.20 |
| H( 2) = | 775.88  |
| H( 3) = | 261.43  |
| H( 4) = | 234.24  |
| TOTAL = | 2867.75 |

**\*\* STATISTICAL ANALYSIS INPUT DATA \*\***

INITIAL NUMBER FOR SUBROUTINE 'GAUSS' 375  
 INITIAL NUMBER FOR SUBROUTINE 'RANDOM' (SETRAND) 375.  
 NUMEROSITY OF THE SAMPLE FOR STATISTICAL ANALYSIS 10000

PROCESS INVENTORY DISTRIBUTION,STEP= 50.

|     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 21  | 35  | 56  | 68  | 94  | 121 | 183 | 248 | 321 | 11  |
| 487 | 569 | 641 | 757 | 883 | 926 | 858 | 787 | 708 | 365 |
| 491 | 340 | 227 | 92  | 29  | 4   | 1   | 0   | 0   | 0   |

MASS PDF

|         |       |
|---------|-------|
| 1692.75 | 0.0   |
| 1742.75 | 0.0   |
| 1792.75 | 0.0   |
| 1842.75 | 0.0   |
| 1892.75 | 0.0   |
| 1942.75 | 0.000 |
| 1992.75 | 0.000 |
| 2042.75 | 0.000 |
| 2092.75 | 0.001 |
| 2142.75 | 0.002 |
| 2192.75 | 0.003 |
| 2242.75 | 0.006 |
| 2292.75 | 0.007 |
| 2342.75 | 0.009 |
| 2392.75 | 0.012 |
| 2442.75 | 0.018 |
| 2492.75 | 0.025 |
| 2542.75 | 0.032 |
| 2592.75 | 0.037 |
| 2642.75 | 0.049 |
| 2692.75 | 0.057 |
| 2742.75 | 0.064 |
| 2792.75 | 0.080 |
| 2842.75 | 0.088 |
| 2892.75 | 0.093 |
| 2942.75 | 0.086 |
| 2992.75 | 0.079 |
| 3042.75 | 0.071 |
| 3092.75 | 0.063 |
| 3142.75 | 0.049 |
| 3192.75 | 0.034 |
| 3242.75 | 0.023 |
| 3292.75 | 0.009 |
| 3342.75 | 0.003 |
| 3392.75 | 0.000 |
| 3442.75 | 0.000 |
| 3492.75 | 0.000 |
| 3542.75 | 0.000 |
| 3592.75 | 0.000 |
| 3642.75 | 0.000 |
| 3692.75 | 0.000 |
| 3742.75 | 0.000 |
| 3792.75 | 0.000 |
| 3842.75 | 0.000 |
| 3892.75 | 0.000 |
| 3942.75 | 0.000 |
| 3992.75 | 0.000 |



4042.75 CcC

- 62 -

|       |    |       |
|-------|----|-------|
| 1642. | 75 | 0.0   |
| 1692. | 75 | 0.0   |
| 1742. | 75 | 0.0   |
| 1792. | 75 | 0.0   |
| 1842. | 75 | 0.0   |
| 1892. | 75 | 0.0   |
| 1942. | 75 | 0.000 |
| 1992. | 75 | 0.000 |
| 2042. | 75 | 0.000 |
| 2092. | 75 | 0.002 |
| 2142. | 75 | 0.004 |
| 2192. | 75 | 0.007 |
| 2242. | 75 | 0.013 |
| 2292. | 75 | 0.020 |
| 2342. | 75 | 0.029 |
| 2392. | 75 | 0.041 |
| 2442. | 75 | 0.059 |
| 2492. | 75 | 0.084 |
| 2542. | 75 | 0.116 |
| 2592. | 75 | 0.153 |
| 2642. | 75 | 0.202 |
| 2692. | 75 | 0.259 |
| 2742. | 75 | 0.323 |
| 2792. | 75 | 0.403 |
| 2842. | 75 | 0.491 |
| 2892. | 75 | 0.584 |
| 2942. | 75 | 0.669 |
| 2992. | 75 | 0.748 |
| 3042. | 75 | 0.819 |
| 3092. | 75 | 0.882 |
| 3142. | 75 | 0.931 |
| 3192. | 75 | 0.965 |
| 3242. | 75 | 0.987 |
| 3292. | 75 | 0.997 |
| 3342. | 75 | 0.999 |
| 3392. | 75 | 1.000 |
| 3442. | 75 | 1.000 |
| 3492. | 75 | 1.000 |
| 3542. | 75 | 1.000 |
| 3592. | 75 | 1.000 |
| 3642. | 75 | 1.000 |
| 3692. | 75 | 1.000 |
| 3742. | 75 | 1.000 |
| 3792. | 75 | 1.000 |
| 3842. | 75 | 1.000 |
| 3892. | 75 | 1.000 |
| 3942. | 75 | 1.000 |
| 3992. | 75 | 1.000 |
| 4042. | 75 | 1.000 |

[illegible]

4092.75 1.000 \*\*\*\*\*

**\*\* STATISTICAL ANALYSIS RESULTS \*\***

|                    |           |
|--------------------|-----------|
| MEAN VALUE         | 2849.8687 |
| STANDARD DEVIATION | 255.9492  |
| PERCENT ST. DEV.   | 8.9811    |
| MEDIAN VALUE       | 2867.7485 |

**CONFIDENCE INTERVALS**

|   | P(X) | X-MEAN  | X       |
|---|------|---------|---------|
| 1 | 2.5  | -528.93 | 2320.94 |
| 2 | 5.0  | -433.08 | 2416.79 |
| 3 | 10.0 | -332.67 | 2517.20 |
| 4 | 20.0 | -209.17 | 2640.70 |
| 5 | 40.0 | 179.53  | 3029.40 |
| 6 | 60.0 | 261.62  | 3111.49 |
| 7 | 80.0 | 321.26  | 3171.13 |
| 8 | 97.5 | 365.57  | 3215.44 |

```

C C C C
COMPUTER CODE CC3

0001 REAL*4 M,MM
0002 DIMENSION SCRITT(2)
0003 DIMENSION M(1),SM(1),X(1),SX(1),Y(1),SY(1)
0004 DIMENSION EM(1),EX(1),EY(1),EQ(1)
0005 DIMENSION XX(3,5),YY(3,5),T(3,5),P(3,5),R(3,5)
0006 DIMENSION XC(3),YC(3),NB(3),EXJ(3),EYJ(3)
0007 DIMENSION LD(62)
0008 DIMENSION CL(20),QL(20)
0009 DIMENSION NUM(62)
0010 DIMENSION ANUM(62),Q(62)
0011 DIMENSION PDF(62)
0012 DIMENSION K7(50)
0013 DIMENSION BM(10)

C
0014 101 FORMAT (5I10)
0015 102 FORMAT (5F10.0)
0016 103 FORMAT (6F10.4)
0017 104 FORMAT (3F10.0)
0018 110 FORMAT (2GA4)

C
0019 200 FORMAT (1H1)
0020 201 FORMAT (////' INITIAL NUMBER FOR SUBROUTINE 'GAUSS' ',15,/,
 1' INITIAL NUMBER FOR SUBROUTINE 'RANDCM' (SETRAND)',F6.1)
0021 202 FORMAT (/,' NUMEROSITY OF THE SAMPLE FOR STATISTICAL ANALYSIS',17)
0022 203 FORMAT (////////,1H , ' ** STATISTICAL ANALYSIS RESULTS **',/,/,
 1' MEAN VALUE ',F10.4,/,
 2' STANDARD DEVIATION ',F10.4,/,
 3' PERCENT ST. DEV. ',F10.4,/,
 4' MEDIAN VALUE ',F10.4)
0023 205 FORMAT (1H ,13,6F10.4)
0024 206 FORMAT (1H ,17,I8,2F15.4)
0025 205 FORMAT (/ ,1H ,8X, 'TOTAL =' ,F9.2,////////)
0026 212 FORMAT (1H ,14,3F15.4)
0027 222 FORMAT (1H , ' MASS PDF',/)
0028 223 FORMAT (1H , ' MASS DISTR.',/)
0029 225 FORMAT (1H ,F10.2,F6.3)
0030 226 FORMAT (1H1 , PROCESS INVENTORY DISTRIBUTION,STEP=' ,F5.0,/)
0031 227 FORMAT (1H ,10I6)
0032 228 FORMAT (1H ,F10.2,F6.3,2X,10CA1)
0033 230 FORMAT (1H ,2CA4)
0034 231 FORMAT (1H)
0035 232 FORMAT (/)
0036 233 FORMAT (1H ,8X, 'H(' ,I2,') =' ,F9.2)

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0037 235 FORMAT (//////, ' PART OF THE INVENTORY CONTAINED IN EACH OUTPUT BATCH'
0038 236 FORMAT (//////, ' CONFIDENCE INTERVALS', ///,
0039 237 FORMAT (15,F8.1,2F12.2)
0040 238 FORMAT (////, ' FOR INCOMPATIBILITY AMONG PROGRAM DIMENSIONS,QMS AND
0041 264 FORMAT (////)
0042 C
0043 301 FORMAT (5I10)
0044 302 FORMAT (5F12.7)
0045 303 FORMAT (5F10.2)
0046 C
0047 C
0048 REAL STAR/'*'/
0049 DIMENSION STARS(100)
0050 DO 501 J=1,100
0051 STARS(J)=STAR
0052 501 CONTINUE
0053 C
0054 Q1=0.
0055 Q2=0.
0056 WRITE (6,200)
0057 READ (5,110) SCRITT
0058 WRITE (6,230) SCRITT
0059 WRITE (6,264)
0060 DO 5 J=1,3
0061 READ (5,110) SCRITT
0062 WRITE (6,230) SCRITT
0063 WRITE (6,231)
0064 READ (5,101) NB(J)
0065 NBB=NB(J)
0066 DO 1 K=1,NBB
0067 READ (5,104) T(J,K),XX(J,K),YY(J,K)
0068 1 CONTINUE
0069 A1=0.
0070 A2=0.
0071 A3=0.
0072 NBB=NB(J)
0073 DO 2 K=1,NBB
0074 A1=A1+T(J,K)*XX(J,K)
0075 A2=A2+T(J,K)*YY(J,K)
0076 A3=A3+T(J,K)
0077 2 CONTINUE
 DO 4 K=1,NBB

```

```

0078 P(J,K)=T(J,K)/A3
0079 4 CONTINUE
0080 XC(J)=A1/A3
0081 YC(J)=A2/A3
0082 WRITE (6,212) (K,(T(J,K),XX(J,K),YY(J,K)),K=1,NBB)
0083 WRITE (6,232)
0084 READ (5,110) SCRITT
0085 WRITE (6,230) SCRITT
0086 WRITE (6,231)
0087 WRITE (6,208) (J,NB(J),XC(J),YC(J))
0088 WRITE (6,264)
0089 5 CONTINUE

C
0090 DO 6 J=1,3
0091 NBB=NB(J)
0092 DO 6 K=1,NBB
0093 XX(J,K)=XX(J,K)-XC(J)
0094 YY(J,K)=YY(J,K)-YC(J)
0095 6 CONTINUE

C
0096 C1=XC(1)
0097 C2=XC(2)
0098 C3=XC(3)
0099 D1=YC(1)
0100 D2=YC(2)
0101 D3=YC(3)

C
0102 WRITE (6,200)
0103 READ (5,110) SCRITT
0104 WRITE (6,230) SCRITT
0105 WRITE (6,264)
0106 READ (5,110) SCRITT
0107 WRITE (6,230) SCRITT
0108 READ (5,110) SCRITT
0109 WRITE (6,230) SCRITT
0110 WRITE (6,231)
0111 READ (5,101) NBATCH
0112 READ (5,103) (M(J),SM(J),X(J),SX(J),Y(J),SY(J)),J=1,NBATCH)
0113 DO 9 J=1,NBATCH
0114 WRITE (6,205) (J,M(J),SM(J),X(J),SX(J),Y(J),SY(J))
0115 9 CONTINUE

C
0116 MM=0.
0117 DET=C1*D2+D3*C2+C3*D1-C1*D3-C2*D1-C3*D2
0118 DO 14 K=1,NBATCH
0119 AM= X(K)*(D2-D3)+C2*(D3-Y(K))+C3*(Y(K)-D2)
0120 BM(K)=M(K)*AM/DET
0121 MM=MM+BM(K)

```

```

0122 14 CONTINUE
0123 WRITE (6,235)
0124 WRITE (6,233) ((K,BM(K)),K=1,NBATCH)
0125 WRITE (6,209) MM

 C ***** ***** ***** *****
 C WRITE (6,200)
0126 READ (5,116) SCRITT
0127 WRITE (6,230) SCRITT
0128 READ (5,101) IX
0129 READ (5,103) RNO
0130 CALL SETRND(RNC)
0131 READ (5,101) NPROVE
0132 PROVE=NPROVE
0133 READ (5,103) QMS,DM
0134 WRITE (6,201) IX,RNO
0135 WRITE (6,202) NPROVE
0136 C=100./FLOAT(NPROVE)
0137 READ (5,101) NCL
0138 READ (5,102) (CL(J),J=1,NCL)
0139 READ (5,101) IPUNCH
0140

 C DO 71 LG=1,62
0141 71 LD(LG)=C
0142

 C LX=INT(QMS/DM)
0143 IF (LX.LT.30) GO TO 50
0144 QMS=30*DM
0145 LMX=62
0146 WRITE (6,238) QMS
0147 GO TO 52
0148
0149 50 CONTINUE
0150 APM=MM-QMS
0151 IF (AMOD(QMS,DM).LT.(DM*0.01)) GO TO 51
0152 LX=LX+1
0153 QMS=LX*DM
0154 51 CONTINUE
0155 LMX=2*LX+2
0156 52 CONTINUE
0157 Q(1)=MM-DM*(FLOAT(LX)+0.5)
0158 DO 55 J=2,LMX
0159 Q(J)=Q(1)+(J-1)*DM
0160 55 CONTINUE

 C DO 13 L=1,NPROVE
0161 DO 31 J=1,3
0162 A1=0.
0163

```

```

0164 A2=0.
0165 A3=0.
0166 NBB=NB(J)
0167 DO 32 K=1,NBB
0168 A4=RANDOM(0.)*T(J,K)
0169 A1=A1+XX(J,K)*A4
0170 A2=A2+YY(J,K)*A4
0171 A3=A3+A4
0172 32 CONTINUE
0173 EXJ(J)=XC(J)+A1/A3
0174 EYJ(J)=YC(J)+A2/A3
0175 31 CONTINUE
0176 EC1=EXJ(1)
0177 EC2=EXJ(2)
0178 EC3=EXJ(3)
0179 ED1=EYJ(1)
0180 ED2=EYJ(2)
0181 ED3=EYJ(3)
0182 415 DET=EC1*ED2+EC2*ED3+EC3*ED1-EC1*ED3-EC2*ED1-EC3*ED2
0183 DO 11 K=1,NBATCH
0184 417 CALL GAUSS(IX,SM(K),M(K),EM(K))
0185 418 CALL GAUSS(IX,SX(K),X(K),EX(K))
0186 419 CALL GAUSS(IX,SY(K),Y(K),EY(K))
0187 420 EQ(K)=EX(K)*(ED2-ED3)+EC2*(ED3-EY(K))+EC3*(EY(K)-ED2)
0188 11 CONTINUE
0189 EQQ=0.
0190 DO 12 K=1,NBATCH
0191 EQQ=EQQ+EQ(K)*EM(K)
0192 12 CONTINUE
0193 EQQ=EQQ/DET
C
0194 Q1=Q1+EQQ
0195 Q2=Q2+EQQ*EQQ
0196 LG=(EQQ-AMM)/DM+2
0197 IF (LG.LT.1) LG=1
0198 IF (LG.GT.LMX) LG=LMX
0199 LD(LG)=LD(LG)+1
0200 13 CONTINUE
C
0201 VMED=Q1/NPROVE
0202 VAR=Q2/NPROVE-VMED*VMED
0203 SDEV=SQRT(VAR)
0204 PERC=(SDEV/VMED)*100.
C
0205 I=1
0206 CCC=CL(I)
0207 NUM(I)=LD(I)
0208 ANUM(I)=NUM(I)*C

```

PS



```

0209 DO 513 J=2,LMX
0210 J1=J-1
0211 NUM(J)=NUM(J1)+LD(J)
0212 ANUM(J)=NUM(J)*C
0213 IF (I.GT.NCL) GO TO 57
0214 IF (ANUM(J).LT.CCC) GO TO 57
0215 QL(I)=Q(J)-DM*(ANUM(J)-CCC)/(ANUM(J)-ANUM(J-1))
0216 I=I+1
0217 CCC=CL(I)
0218 57 CONTINUE
0219 513 CONTINUE
C
0220 WRITE (6,203) VMED,SDEV,PERC,MM
0221 WRITE (6,236)
0222 DO 59 J=1,NCL
0223 QC=QL(J)-VMED
0224 QC=QL(J)-MM
0225 WRITE (6,237) (J,CL(J),QC,QL(J))
0226 59 CONTINUE
C
0227 WRITE (6,226) DM
0228 LMX1=LMX-1
0229 WRITE (6,227) (LD(LG),LG=1,LMX)
0230 I=LD(1)
0231 DO 15 J=2,LMX
0232 K=LD(J)
0233 I=MAX0(I,K)
0234 15 CONTINUE
0235 DO 16 J=2,LMX1
0236 K7(J)=LD(J)*50/I
0237 16 CONTINUE
C
0238 DO 520 J=1,LMX
0239 PCF(J)=FLOAT(LD(J))/PROVE
0240 520 CONTINUE
C
0241 IF (IPUNCH.NE.777) GO TO 521
0242 IN=1
0243 DO 60 J=1,LMX
0244 IF (PDF(J).NE.0.) GO TO 61
0245 IN=IN+1
0246 60 CONTINUE
0247 61 CONTINUE
0248 IL=LMX
0249 DO 62 J=1,LMX
0250 K=LMX-J+1
0251 IF (PDF(K).NE.0.) GO TO 63
0252 IL=IL-1

```

```
0253 62 CONTINUE
0254 63 CONTINUE
0255 LU=IL-IN+1
0256 WRITE (7,301) LU
0257 WRITE (7,303) (Q(IN),VMED,SDEV)
0258 WRITE (7,302) (PDF(J),J=IN,IL)
0259 521 CONTINUE
C
0260 WRITE (6,264)
0261 WRITE (6,222)
0262 DO 500 JJ=2,LMX1
0263 LLL=K7(JJ)
0264 IF (LLL.LE.0) GO TO 499
0265 WRITE (6,228) (Q(JJ),PDF(JJ),(STARS(J),J=1,LLL))
0266 GO TO 500
0267 499 CONTINUE
0268 WRITE (6,225) (Q(JJ),PDF(JJ))
0269 500 CONTINUE
C
0270 WRITE (6,200)
0271 WRITE (6,227) (NUM(J),J=1,LMX)
0272 WRITE (6,264)
C
0273 WRITE (6,223)
0274 DO 511 J=2,LMX
0275 PDF(J)=PDF(J-1)+PDF(J)
0276 511 CONTINUE
C
0277 LM=NUM(LMX)
0278 F=100./UM
0279 DO 514 LG=1,LMX
0280 LD(LG)=NUM(LG)*F
0281 514 CONTINUE
0282 DO 515 JJ=1,LMX
0283 LLL=LD(JJ)
0284 IF (LLL.LE.0) GO TO 516
0285 WRITE (6,228) (Q(JJ),PDF(JJ),(STARS(J),J=1,LLL))
0286 GO TO 515
0287 516 CONTINUE
0288 WRITE (6,225) (Q(JJ),PDF(JJ))
0289 515 CONTINUE
C
0290 STOP
0291 END
```

The subroutines

SETRAND (RANDOM)

GAUSS

RANDU

are listed together with the CC2 code

\*\*\* LIST OF THE DATA CARDS USED FOR THE "CC3" SAMPLE PROGRAM \*\*\*

```

** INPUT BATCH DATA **
CANCU REACTOR
BATCH PU MASS (G) PU-41 CONC. PU-42 CONC.
4
3434.4 3.41 0.585
3218.4 3.67 1.05
3381.0 3.81 1.11
3386.7 3.72 1.65
REACTOR BATCHES MEAN VALUES
VAK REACTOR
BATCH PU MASS (G) PU-41 CONC. PU-42 CONC.
4
3103.5 7.53 1.57
2109.6 8.08 2.30
4309.0 6.18 2.42
702.7 7.74 1.78
REACTOR BATCHES MEAN VALUES
TRIND REACTOR
BATCH PU MASS (G) PU-41 CONC. PU-42 CONC.
2
3420.3 7.18 1.19
3149.8 5.94 0.90
REACTOR BATCHES MEAN VALUES
** OUTPUT BATCH DATA **
PU-MASS (G) PU-41 CONC. PU-42 CONC.
NO. VALUE ST. DEV. PERCENT ST. DEV. PERCENT ST. DEV.
1
5415.7 20.0785 6.575 0.022875 1.250 0.01625
** STATISTICAL ANALYSIS INPUT DATA **
357
10000
900. 8 50.
2.5 5.0 10. 20. 80.
90. 95. 97.5
777

```

NPROVE  
CMS DM

REQUESTED PUNCHED CARDS

\*\* INPUT BATCH DATA \*\*

CANDU REACTOR

| BATCH | PU MASS (G) | PU-41 CONC. | PU-42 CONC. |
|-------|-------------|-------------|-------------|
| 1     | 3434.3999   | 3.4100      | 0.9850      |
| 2     | 3218.3999   | 3.6700      | 1.0500      |
| 3     | 3381.0000   | 3.8100      | 1.1100      |
| 4     | 3386.7000   | 3.7200      | 1.0900      |

| REACTOR | BATCHES | MEAN   | VALUES |
|---------|---------|--------|--------|
| 1       | 4       | 3.6514 | 1.0586 |

VAK REACTOR

| BATCH | PU MASS (G) | PU-41 CONC. | PU-42 CONC. |
|-------|-------------|-------------|-------------|
| 1     | 3103.5000   | 7.5300      | 1.9700      |
| 2     | 2109.5999   | 8.0800      | 2.3000      |
| 3     | 4309.0000   | 8.1800      | 2.4200      |
| 4     | 702.7000    | 7.7400      | 1.7800      |

| REACTOR | BATCHES | MEAN   | VALUES |
|---------|---------|--------|--------|
| 2       | 4       | 7.9318 | 2.2147 |

TRINO REACTOR

| BATCH | PU MASS (G) | PU-41 CONC. | PU-42 CONC. |
|-------|-------------|-------------|-------------|
| 1     | 3420.2998   | 7.1800      | 1.1900      |
| 2     | 3149.7998   | 5.9400      | 0.9000      |

| REACTOR | BATCHES | MEAN   | VALUES |
|---------|---------|--------|--------|
| 3       | 2       | 6.5855 | 1.0510 |

\*\* OUTPUT BATCH DATA \*\*

| NO. | PU-MASS (G) |          | PU-41 CONC. |          | PU-42 CONC. |          |
|-----|-------------|----------|-------------|----------|-------------|----------|
|     | VALUE       | ST. DEV. | PERCENT     | ST. DEV. | PERCENT     | ST. DEV. |
| 1   | 5415.6992   | 20.0785  | 6.5750      | 0.0329   | 1.2500      | 0.0162   |

PART OF THE INVENTORY CONTAINED IN EACH OUTPUT BATCH

H( 1) = 443.10

TOTAL = 443.10

**\*\* STATISTICAL ANALYSIS INPUT DATA \*\***

INITIAL NUMBER FOR SUBROUTINE 'GAUSS' 357  
 INITIAL NUMBER FOR SUBROUTINE 'RANDOM' (SETRAND) 357.  
 NUMEROSITY OF THE SAMPLE FOR STATISTICAL ANALYSIS 10000

**\*\* STATISTICAL ANALYSIS RESULTS \*\***

MEAN VALUE 431.8501  
 STANDARD DEVIATION 308.2153  
 PERCENT ST. DEV. 71.3769  
 MEDIAN VALUE 443.1021

**CONFIDENCE INTERVALS**

|   | P(X) | X-MEAN  | X       |
|---|------|---------|---------|
| 1 | 2.5  | -636.26 | -204.41 |
| 2 | 5.0  | -566.10 | -134.25 |
| 3 | 10.0 | -453.18 | -21.33  |
| 4 | 20.0 | -296.56 | 135.29  |
| 5 | 40.0 | -254.69 | 686.54  |
| 6 | 60.0 | 351.89  | 823.74  |
| 7 | 80.0 | 473.84  | 905.69  |
| 8 | 97.5 | 528.94  | 969.79  |

PROCESS INVENTORY DISTRIBUTION, STEP= 50.

|     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 0   | 1   | 8   | 18  | 50  | 90  | 151 | 191 | 219 | 216 |
| 265 | 321 | 328 | 413 | 439 | 475 | 546 | 624 | 680 | 650 |
| 631 | 569 | 515 | 458 | 385 | 397 | 323 | 328 | 278 | 212 |
| 136 | 70  | 12  | 1   | 0   | 0   | 0   | 0   | 0   | 0   |

| MASS    | PDF   |
|---------|-------|
| -431.90 | 0.000 |
| -381.90 | 0.001 |
| -331.90 | 0.002 |
| -281.90 | 0.005 |
| -231.90 | 0.009 |
| -181.90 | 0.015 |
| -131.90 | 0.019 |
| -81.90  | 0.022 |
| -31.90  | 0.022 |
| 18.10   | 0.026 |
| 68.10   | 0.032 |
| 118.10  | 0.033 |
| 168.10  | 0.041 |
| 218.10  | 0.044 |
| 268.10  | 0.047 |
| 318.10  | 0.055 |
| 368.10  | 0.062 |
| 418.10  | 0.068 |
| 468.10  | 0.065 |
| 518.10  | 0.063 |
| 568.10  | 0.057 |
| 618.10  | 0.051 |
| 668.10  | 0.046 |
| 718.10  | 0.038 |
| 768.10  | 0.040 |
| 818.10  | 0.032 |
| 868.10  | 0.033 |
| 918.10  | 0.028 |
| 968.10  | 0.021 |
| 1018.10 | 0.014 |
| 1068.10 | 0.007 |
| 1118.10 | 0.001 |
| 1168.10 | 0.000 |
| 1218.10 | 0.0   |
| 1268.10 | 0.0   |
| 1318.10 | 0.0   |



|      |      |      |       |       |       |       |       |      |      |
|------|------|------|-------|-------|-------|-------|-------|------|------|
| 1209 | 1530 | 1858 | 2271  | 2710  | 3185  | 3731  | 4355  | 5035 | 5685 |
| 6316 | 6885 | 7400 | 7858  | 8243  | 8640  | 8963  | 9291  | 9569 | 9781 |
| 9917 | 9987 | 9999 | 10000 | 10000 | 10000 | 10000 | 10000 |      |      |

MASS DISTR.

|         |       |       |
|---------|-------|-------|
| -481.90 | 0.0   |       |
| -431.90 | 0.000 |       |
| -381.90 | 0.001 |       |
| -331.90 | 0.003 |       |
| -281.90 | 0.008 |       |
| -231.90 | 0.017 | *     |
| -181.90 | 0.032 | ***   |
| -131.90 | 0.051 | ***** |
| -81.90  | 0.073 | ***** |
| -31.90  | 0.094 | ***** |
| 18.10   | 0.121 | ***** |
| 68.10   | 0.153 | ***** |
| 118.10  | 0.186 | ***** |
| 168.10  | 0.227 | ***** |
| 218.10  | 0.271 | ***** |
| 268.10  | 0.318 | ***** |
| 318.10  | 0.373 | ***** |
| 368.10  | 0.435 | ***** |
| 418.10  | 0.503 | ***** |
| 468.10  | 0.568 | ***** |
| 518.10  | 0.632 | ***** |
| 568.10  | 0.688 | ***** |
| 618.10  | 0.748 | ***** |
| 668.10  | 0.786 | ***** |
| 718.10  | 0.824 | ***** |
| 768.10  | 0.864 | ***** |
| 818.10  | 0.896 | ***** |
| 868.10  | 0.929 | ***** |
| 918.10  | 0.957 | ***** |
| 968.10  | 0.978 | ***** |
| 1018.10 | 0.992 | ***** |
| 1068.10 | 0.999 | ***** |
| 1118.10 | 1.000 | ***** |
| 1168.10 | 1.000 | ***** |
| 1218.10 | 1.000 | ***** |
| 1268.10 | 1.000 | ***** |
| 1318.10 | 1.000 | ***** |
| 1368.10 | 1.000 | ***** |

## COMPUTER CODE PUF

```

0001 IMPLICIT REAL*8(A-H,C-Z)
0002 DIMENSION V1(900),V2(900),VX(900),T(900)
0003 DIMENSION IT(900)
0004 DIMENSION KS(900)
0005 DIMENSION QL(20),CL(20)
0006 DIMENSION Q(900)
0007 DIMENSION D4(900),V4(900)
0008 DIMENSION STARS(100)
0009 REAL*4 SUM/'+'/'
0010 REAL*4 DIFF1/'1-2'/'
0011 REAL*4 DIFF2/'2-1'/'
0012 REAL*4 ALT/'ALT'/'
0013 REAL*4 STAR/'*'/'
0014 REAL*4 CONV
0015 101 FORMAT (5I10)
0016 102 FORMAT (5F10.0)
0017 104 FORMAT (5F12.0)
0018 105 FORMAT (A3)
0019 200 FORMAT (1H1)
0020 201 FORMAT (///)
0021 202 FORMAT (1H,10F11.8)
0022 203 FORMAT (1H,10I5)
0023 204 FORMAT (///,1H,2F15.5)
0024 209 FORMAT (1H1,
1' CONVOLUTIONS OF A SEQUENCE OF PROBABILITY DENSITY FUNCTIONS',/,
2' (P.D.F.) GIVEN IN HISTOGRAM FORM FOR EACH HISTOGRAM THE',/,
3' VALUE IS FIX AND EQUAL TO',F6.2)
0025 210 FORMAT (' RELEVANT DATA OF THE P.D.F. *1*',/)
0026 211 FORMAT (//////,' RELEVANT DATA OF THE P.D.F. *2*',/)
0027 212 FORMAT (//////,7X,A3,' CONVOLUTION REQUIRED BETWEEN P.D.F. *1* AND
1 P.D.F. *2*')
0028 213 FORMAT (1H1,' RESULT OF THE CONVOLUTION ',A3,//////)
0029 214 FORMAT (' RESULTING P.D.F.',///)
0030 215 FORMAT (///,' RESULTING DISTRIBUTION FUNCTION',///)
0031 216 FORMAT (//,110,' NUMBER OF THE HISTOGRAM POINTS',
1/,F10.2,' ABSCISSA OF THE FIRST POINT',
2/,F10.2,' MEAN VALUE OF THE DISTRIBUTION',
3/,F10.3,' STANDARD DEVIATION OF THE MEAN',///)
0032 217 FORMAT (//////,' RELEVANT DATA',/)
0033 222 FORMAT (1H,,' MASS PDF',/)
0034 223 FORMAT (1H,,' MASS DISTR.',/)
0035 225 FORMAT (1H,10F10.2,F7.4)
0036 228 FORMAT (1H,10F10.2,F7.4,2X,100A1)

```

```

0037 236 FORMAT (' CONFIDENCE INTERVALS', ///,
0038 1' P(X) X-MEAN X' ///)
0039 237 FORMAT (15,F8.1,2F12.2)
0040 240 FORMAT (1H ,F10.6,101A1)
0041 C
0042 DO 501 J=1,100
0043 STARS(J)=STAR
0044 501 CONTINUE
0045 C
0046 READ (5,102) PASSO
0047 WRITE (6,209) PASSO
0048 ASSIGN 50 TO IADD
0049 READ (5,101) NCL
0050 READ (5,102) (CL(J),J=1,NCL)
0051 C
0052 READ (5,101) N1
0053 IF (N1.NE.999) GO TO 40
0054 C
0055 ASSIGN 51 TO IADD
0056 N2=N1
0057 C
0058 52 CONTINUE
0059 READ (5,102) Q2MED,Q2SD
0060 DD=PASSO/Q2SD
0061 NN=3./DD
0062 IF (NN.LT.1) NN=1
0063 X=-NN*DD
0064 CALL NDTR(X,P,D)
0065 D4(1)=P
0066 V2(1)=P
0067 NBX=2*NN+1
0068 DO 27 J=2,NBX
0069 J1=J-1
0070 X=(J1-NN)*DD
0071 CALL NDTR(X,P,D)
0072 D4(J)=P
0073 V2(J)=P-D4(J1)
0074 27 CONTINUE
0075 N2=NBX+1
0076 Q2=Q2MED-(FLCAT(N2)-0.5)*PASSO
0077 V2(N2)=1.-D4(NBX)
0078 D4(N2)=1.
0079 GO TO IADD,(50,51)
0080 C
0081 51 CONTINUE
0082 N1=N2
0083 Q1=Q2
0084 Q1SD=Q2SD

```

```

0078 Q1MED=Q2MED
0079 DO 54 J=1,N1
0080 V1(J)=V2(J)
0081 54 CONTINUE
0082 ASSIGN 50 TO IADD
0083 GO TO 41
C
0084 40 CONTINUE
0085 READ (5,102) Q1,Q1MED,Q1SD
0086 READ (5,104) (V1(J),J=1,N1)
C
C
C
0087 41 CONTINUE
0088 READ (5,105) CONV
0089 IF (CONV.EQ.AL1) GO TO 59
0090 READ (5,101) ICONF
0091 READ (5,101) ISTAR
C
0092 READ (5,101) N2
0093 IF (N2.EQ.999) GO TO 53
C
0094 READ (5,102) Q2,Q2MED,Q2SD
0095 READ (5,104) (V2(J),J=1,N2)
C
0096 50 CONTINUE
0097 WRITE (6,200)
0098 WRITE (6,210)
0099 WRITE (6,216) N1,Q1,Q1MED,Q1SD
0100 WRITE (6,202) (V1(J),J=1,N1)
0101 WRITE (6,211)
0102 WRITE (6,216) N2,Q2,Q2MED,Q2SD
0103 WRITE (6,202) (V2(J),J=1,N2)
0104 WRITE (6,212) CONV
C
0105 IF (CONV.NE.SUP) GO TO 58
C
0106 24 CONTINUE
0107 IF (N2.GE.N1) GO TO 4
C
C N1 MUST BE LOWER THAN N2
0108 DO 1 J=1,N1
0109 1 VX(J)=V1(J)
0110 DO 2 J=1,N2
0111 2 V1(J)=V2(J)
0112 DO 3 J=1,N1
0113 3 V2(J)=VX(J)
0114 NX=N1

```

```

0115 N1=N2
0116 N2=NX
0117 QX=Q1
0118 Q1=Q2
0119 Q2=QX
0120 QY=Q1MED
0121 Q1MED=Q2MED
0122 Q2MED=QY

C
0123 4 CONTINUE
0124 A=N1+N2
0125 TT(1)=0.
0126 E=0.
0127 V=0.
0128 DO 10 M=2,N
0129 L1=1
0130 L2=N1
0131 IF ((M-1).LT.N1) L2=M-1
0132 IF ((M-N2).GT.1) L1=M-N2
0133 T(M)=0
0134 DO 9 L=L1,L2
0135 M1=M-L
0136 T(M)=T(M)+V1(L)*V2(M1)
0137 9 CONTINUE
0138 MM=M-1
0139 TT(M)=TT(MM)+T(M)
0140 R=MM
0141 E=E+R*T(M)
0142 V=V+R*R*T(M)
0143 10 CONTINUE

C
0144 Q1=Q1+Q2
0145 Q1MED=Q1+(E-1.)*PASSE
0146 V=DSQRT(V-E*E)
0147 Q1SD=V*PASSO
0148 N1=N-1
0149 DO 43 J=1,N1
0150 V1(J)=T(J+1)
0151 43 CONTINUE
0152 WRITE (6,213) LDI V
0153 WRITE (6,214)
0154 WRITE (6,212) (V1(M),M=1,N1)
0155 WRITE (6,215)
0156 WRITE (6,212) (TT(M),M=2,N)
0157 WRITE (6,217)
0158 WRITE (6,216) N1,Q1,Q1MED,Q1SD

C
0159 Q(1)=Q1

```

```

0160 DO 75 J=2,N1
0161 Q(J)=Q1+PASSO*FLCAT(J-1)
0162 75 CONTINUE
0163 DO 76 J=1,N1
0164 TT(J)=TT(J+1)
0165 76 CONTINUE
C
0166 IF (ICONF.NE.777) GO TO 20
0167 I=1
0168 CCC=CL(I)/100.
0169 DO 70 J=2,N1
0170 JJ=J-1
0171 IF (TT(J).LT.CCC) GO TO 70
0172 QL(I)=Q(J)-PASSO*(TT(J)-CCC)/(TT(J)-TT(J-1))
0173 I=I+1
0174 IF (I.GT.NCL) GO TO 71
0175 CCC=CL(I)/100.
0176 70 CONTINUE
0177 71 CONTINUE
0178 WRITE (6,213) CONV
0179 WRITE (6,236)
0180 DO 78 J=1,NCL
0181 QD=QL(J)-QIMED
0182 WRITE (6,237) (J,CL(J),QD,QL(J))
0183 78 CONTINUE
0184 20 CONTINUE
C
0185 IF (ISTARS.NE.888) GO TO 19
C
0186 PLOT NEL CASO DELLE CONV = +
0187 WRITE (6,200)
0188 CALL STELLE(V1,N1, 50,KS)
0189 WRITE (6,222)
0190 DO 80 J=1,N1
0191 LLL=KS(J)
0192 IF (LLL.LE.0) GO TO 81
0193 WRITE (6,228) (Q(J),V1(J),(STARS(JJ),JJ=1,LLL))
0194 GO TO 80
0195 81 CONTINUE
0196 WRITE (6,225) (Q(J),V1(J))
C
0197 WRITE (6,200)
0198 CALL STELLE(TT,N1,100,KS)
0199 WRITE (6,223)
0200 DO 82 J=1,N1
0201 LLL=KS(J)
0202 IF (LLL.LE.0) GO TO 83
0203 WRITE (6,228) (Q(J),TT(J),(STARS(JJ),JJ=1,LLL))

```

```

0204 GO TO 82
0205 83 CONTINUE
0206 WRITE (6,225) (Q(J),T1(J))
0207 82 CONTINUE
0208 19 CONTINUE
0209 GO TO 41

C
C
C
C
C
C
0210 58 CONTINUE
0211 IF (CONV.EQ.0.DIFF1) GO TO 57

C
0212 DO 66 J=1,N1
0213 66 VX(J)=V1(J)
0214 DO 64 J=1,N2
0215 64 V1(J)=V2(J)
0216 DO 65 J=1,N1
0217 65 V2(J)=VX(J)
0218 NX=N1
0219 N1=N2
0220 N2=NX
0221 QX=Q1
0222 Q1=Q2
0223 Q2=QX
0224 QY=Q1MED
0225 Q1MED=Q2MED
0226 Q2MED=QY
0227 QZ=Q1SD
0228 Q1SD=Q2SD
0229 Q2SD=QZ
0230 57 CONTINUE

C
0231 E=0.
0232 V=0.
0233 N=N1+N2-1
0234 DO 12 MN=1,N
0235 R=MN
0236 M=MN-N2
0237 L1=MAX0(1,(1-M))
0238 L2=MIN0(N2,(N1-M))
0239 T(MN)=0.
0240 DO 11 L=L1,L2
0241 LP=L+M
0242 T(MN)=T(MN)+V1(LP)*V2(L)
0243 11 CONTINUE

```

```

0244 E=E+R*T(MN)
0245 V=V+R*R*T(MN)
0246 12 CONTINUE
0247 TT(1)=T(1)
0248 DO 13 M=2,N
0249 M1=M-1
0250 TT(M)=TT(M1)+T(M)
0251 13 CONTINUE
C
0252 Q1=Q2-Q1-PASSO*FLOAT(N1-1)
0253 Q1MED=Q1+(E-1.)*PASSO
0254 V=DSORT(V-E*E)
0255 Q1SD=V*PASSO
0256 N1=N
0257 DO 14 J=1,N
0258 V1(J)=T(J)
0259 14 CONTINUE
C
0260 WRITE (6,213) CONV
0261 WRITE (6,214)
0262 WRITE (6,202) (V1(M),M=1,N1)
0263 WRITE (6,215)
0264 WRITE (6,202) (TT(M),M=1,N)
0265 WRITE (6,217)
0266 WRITE (6,216) N1,Q1,Q1MED,Q1SD
C
0267 Q(1)=Q1
0268 DO 74 J=2,N1
0269 Q(J)=Q1+PASSO*FLOAT(J-1)
0270 74 CONTINUE
C
0271 IF (ICONF.NE.777) GO TO 22
0272 I=1
0273 CCC=CL(I)/100.
0274 DO 72 J=2,N1
0275 J1=J-1
0276 IF (TT(J).LT.CCC) GO TO 72
0277 QL(I)=Q(J)-PASSO*(TT(J)-CCC)/(TT(J)-TT(J-1))
0278 I=I+1
0279 IF (I.GT.NCL) GO TO 73
0280 CCC=CL(I)/100.
0281 72 CONTINUE
0282 73 CONTINUE
0283 WRITE (6,213) CONV
0284 WRITE (6,236)
0285 DO 77 J=1,NCL
0286 QD=QL(J)-Q1MED
0287 WRITE (6,237) (J,CL(J),QD,QL(J))

```



```

0288 77 CONTINUE
0289 22 CONTINUE
C
0290 IF (ISTARS.NE.888) GO TO 16
0291 WRITE (6,200)
0292 CALL STELLE (T,N,50,KS)
0293 WRITE (6,222)
0294 DO 60 J=1,N
0295 LLL=KS(J)
0296 IF (LLL.LE.0) GO TO 61
0297 WRITE (6,228) (Q(J),V1(J),(STARS(JJ),JJ=1,LLL))
0298 GO TO 60
0299 61 CONTINUE
0300 WRITE (6,225) (Q(J),V1(J))
0301 60 CONTINUE
C
0302 WRITE (6,200)
0303 CALL STELLE (TT,N,100,KS)
0304 WRITE (6,223)
0305 DO 62 J=1,N
0306 LLL=KS(J)
0307 IF (LLL.LE.0) GO TO 63
0308 WRITE (6,228) (Q(J),T1(J),(STARS(JJ),JJ=1,LLL))
0309 GO TO 62
0310 63 CONTINUE
0311 WRITE (6,225) (Q(J),T1(J))
0312 62 CONTINUE
0313 16 CONTINUE
0314 GO TO 41
0315 55 CONTINUE
0316 STOP
0317 END

```

```

0001 SUBROUTINE STELLE (T,N,NORM,K)
0002 IMPLICIT REAL*8(A-H,C-Z)
0003 DIMENSION T(500),K(500)
0004 B=T(1)
0005 DO 1 J=2,N
0006 TJ=T(J)
0007 B=DMAX1(B,TJ)
0008 1 CONTINUE
0009 ORM=NCRM
0010 DO 2 J=1,N
0011 C=(T(J)/B)*ORM
0012 K(J)=C
0013 2 CONTINUE
0014 RETURN
0015 END

```

```

CNDTR 10
CNDTR 20
CNDTR 30
CNDTR 40
CNDTR 50
CNDTR 60
CNDTR 70
CNDTR 80
CNDTR 90
CNDTR 100
CNDTR 110
CNDTR 120
CNDTR 130
CNDTR 140
CNDTR 150
CNDTR 160
CNDTR 170
CNDTR 180
CNDTR 190
CNDTR 200
CNDTR 210
CNDTR 220
CNDTR 230
CNDTR 240
CNDTR 250
CNDTR 260
CNDTR 270
CNDTR 280
CNDTR 290
CNDTR 300
CNDTR 310
CNDTR 320
CNDTR 330
CNDTR 340
CNDTR 350
CNDTR 360
CNDTR 370
CNDTR 380
CNDTR 390
CNDTR 400
CNDTR 410
CNDTR 420
CNDTR 430
CNDTR 440
CNDTR 450

SUBROUTINE NDTR
PURPOSE
 COMPUTES Y = P(X) = PROBABILITY THAT THE RANDOM VARIABLE U,
 DISTRIBUTED NORMALLY(0,1), IS LESS THAN OR EQUAL TO X.
 F(X), THE ORDINATE OF THE NORMAL DENSITY AT X, IS ALSO
 COMPUTED.

USAGE
 CALL NDTR(X,P,D)

DESCRIPTION OF PARAMETERS
 X--INPUT SCALAR FOR WHICH P(X) IS COMPUTED.
 P--OUTPUT PROBABILITY.
 D--OUTPUT DENSITY.

REMARKS
 MAXIMUM ERROR IS 0.0000007.

SUBROUTINES AND SUBPROGRAMS REQUIRED
 NONE

METHOD
 BASED ON APPROXIMATIONS IN C. HASTINGS, APPROXIMATIONS FOR
 DIGITAL COMPUTERS, PRINCETON UNIV. PRESS, PRINCETON, N.J.,
 1955. SEE EQUATION 26.2.17, HANDBOOK OF MATHEMATICAL
 FUNCTIONS, ABRAMOWITZ AND STEGUN, DOVER PUBLICATIONS, INC.,
 NEW YORK.

CNDTR 360
CNDTR 370
CNDTR 380
CNDTR 390
CNDTR 400
CNDTR 410
CNDTR 420
CNDTR 430
CNDTR 440
CNDTR 450

SUBROUTINE NDTR(X,P,D)
 IMPLICIT REAL*8(A-H,C-Z)

 AX=DABS(X)
 T=1.0/(1.0+0.2316419*AX)
 D=0.3989423*DEXP(-X*X/2.0)
 P = 1.0 - D*T*(((1.330274*T - 1.821256)*T + 1.781478)*T -
1 0.3565638)*T + 0.3193815)
 IF(X)1,2,2
1 P=1.0-P
2 RETURN
END

```

0001  
0002  
  
0003  
0004  
0005  
0006  
  
0007  
0008  
0009  
0010

\*\*\* LIST OF THE DATA CARDS USED FOR THE 'MUF' SAMPLE PROGRAM \*\*\*

50.  
2.5 8  
90.0 5.0 10.0 20.0 80.0  
95.0 97.5

7802. 27.8

+ 777  
688  
31

CONFIDENCE LIMITS REQUIRED  
PLOT REQUIRED

|           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|
| 1942.75   | 2849.87   | 255.95    |           |           |
| 0.0001000 | 0.0002000 | 0.0002000 | 0.0011000 | 0.0021000 |
| 0.0035000 | 0.0050000 | 0.0068000 | 0.0094000 | 0.0121000 |
| 0.0183000 | 0.0240000 | 0.0321000 | 0.0369000 | 0.0487000 |
| 0.0569000 | 0.0640000 | 0.0797000 | 0.0883000 | 0.0926000 |
| 0.0858000 | 0.0789999 | 0.0707999 | 0.0627000 | 0.0491000 |
| 0.0340000 | 0.0227000 | 0.0092000 | 0.0029000 | 0.0004000 |
| 0.0001000 |           |           |           |           |

+ 777  
688  
33

CONFIDENCE LIMITS REQUIRED  
PLOT REQUIRED

|           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|
| -431.90   | 431.85    | 308.22    |           |           |
| 0.0001000 | 0.0008000 | 0.0018000 | 0.0050000 | 0.0090000 |
| 0.0151000 | 0.0191000 | 0.0219000 | 0.0216000 | 0.0265000 |
| 0.0321000 | 0.0328000 | 0.0413000 | 0.0439000 | 0.0475000 |
| 0.0546000 | 0.0624000 | 0.0680000 | 0.0690000 | 0.0631000 |
| 0.0569000 | 0.0515000 | 0.0458000 | 0.0395000 | 0.0397000 |
| 0.0323000 | 0.0318000 | 0.0278000 | 0.0212000 | 0.0136000 |
| 0.0070000 | 0.0012000 | 0.0001000 |           |           |

PU/1 3  
PU/1 3C  
PU/1 3C  
PU/1 3C  
PU/1 3C  
PU/1 3C  
PU/1 3C  
PU/1 3C

4-1 777  
688  
999

CONFIDENCE LIMITS REQUIRED  
PLOT REQUIRED

11190. 141.  
ALT

CONVOLUTIONS OF A SEQUENCE OF PROBABILITY DENSITY FUNCTIONS  
(P.D.F.) GIVEN IN HISTOGRAM FORM. FOR EACH HISTOGRAM THE  
VALUE IS FIX AND EQUAL TO 50.00

RELEVANT DATA OF THE P.D.F. \*1\*

4 NUMBER OF THE HISTOGRAM POINTS  
7627.00 ABSCISSA OF THE FIRST POINT  
7802.00 MEAN VALUE OF THE DISTRIBUTION  
27.800 STANDARD DEVIATION OF THE MEAN

0.03604401 0.46395619 0.46395579 0.03604401

RELEVANT DATA OF THE P.D.F. \*2\*

31 NUMBER OF THE HISTOGRAM POINTS  
1942.75 ABSCISSA OF THE FIRST POINT  
2849.87 MEAN VALUE OF THE DISTRIBUTION  
255.950 STANDARD DEVIATION OF THE MEAN

0.00010000 0.00030000 0.00020000 0.00110000 0.00210000 0.00350000 0.00560000 0.00680000 0.00940000 0.01210000  
0.01830000 0.02480000 0.03210000 0.03690000 0.04870000 0.05690000 0.06410000 0.07570000 0.08830000 0.09260000  
0.08580000 0.07865590 0.07079990 0.06270000 0.04910000 0.03400000 0.02270000 0.00920000 0.00290000 0.00040000  
0.00010000

\* CONVOLUTION REQUIRED BETWEEN P.D.F. \*1\* AND P.D.F. \*2\*

# RESULT OF THE CONVOLUTION +

## RESULTING P<sub>0</sub>D<sub>0</sub>F<sub>0</sub>

0.00000360 0.00005721 0.00019279 0.00027523 0.00068965 0.00161802 0.00283965 0.00454279 0.00621802 0.00815407  
 0.01087976 0.01533697 0.02158965 0.02838673 0.03466220 0.04292255 0.05263420 0.06176673 0.07195746 0.08359278  
 0.08989492 0.08878909 0.08221030 0.07471386 0.06544500 0.05564769 0.04163290 0.02840767 0.01613022 0.00644648  
 0.00166626 0.00033651 0.00006081 0.00000360

## RESULTING DISTRIBUTION FUNCTION

0.00000360 0.00006081 0.00025360 0.00052884 0.00121848 0.00283651 0.00567615 0.01021895 0.01643697 0.02459104  
 0.03547079 0.05080776 0.07239741 0.10078614 0.13544834 0.17837089 0.23100509 0.29177182 0.36372228 0.44731499  
 0.53726591 0.62599900 0.70826930 0.78292316 0.84946766 0.90511535 0.94674825 0.97515591 0.99128613 0.99773261  
 0.99959888 0.99992538 0.99999620 0.99999980

## RELEVANT DATA

34 NUMBER OF THE HISTOGRAM POINTS  
 9569.75 ABSCISSA OF THE FIRST POINT  
 10555.33 MEAN VALUE OF THE DISTRIBUTION  
 230.436 STANDARD DEVIATION OF THE MEAN

# RESULT OF THE CONVOLUTION +

## CONFIDENCE INTERVALS

|   | P(X) | X-MEAN  | X        |
|---|------|---------|----------|
| 1 | 2.5  | -533.71 | 10021.63 |
| 2 | 5.0  | -438.22 | 10117.12 |
| 3 | 10.0 | -336.97 | 10218.37 |
| 4 | 20.0 | -215.04 | 10340.30 |
| 5 | 80.0 | 177.25  | 10732.58 |
| 6 | 90.0 | 255.62  | 10815.15 |
| 7 | 95.0 | 320.14  | 10875.47 |
| 8 | 97.5 | 363.93  | 10919.27 |



[illegible]

RELEVANT DATA OF THE P.D.F. \*1\*

34 NUMBER OF THE HISTOGRAM POINTS  
9569.75 ABSCISSA OF THE FIRST POINT  
10555.33 MEAN VALUE OF THE DISTRIBUTION  
230.436 STANDARD DEVIATION OF THE MEAN

0.00000360 0.00005721 0.00019279 0.00027523 0.00068965 0.00161802 0.00283965 0.00454279 0.00621802 0.00815407  
0.01087976 0.01532657 0.02158965 0.02838873 0.03466220 0.04292255 0.05263420 0.06076673 0.07195046 0.08359270  
0.08989492 0.08878909 0.08221030 0.07471386 0.06654450 0.05564769 0.04163290 0.02846767 0.01613022 0.00644648  
0.00186626 0.00033651 0.00006081 0.00000360

RELEVANT DATA OF THE P.D.F. \*2\*

33 NUMBER OF THE HISTOGRAM POINTS  
-431.90 ABSCISSA OF THE FIRST POINT  
431.85 MEAN VALUE OF THE DISTRIBUTION  
308.220 STANDARD DEVIATION OF THE MEAN

0.00010000 0.00080000 0.00180000 0.00500000 0.00900000 0.01510000 0.01910000 0.02190000 0.02160000 0.02650000  
0.03210000 0.03280000 0.04130000 0.04390000 0.04750000 0.05460000 0.06240000 0.06800000 0.06500000 0.06310000  
0.05690000 0.05150000 0.04580000 0.03850000 0.03970000 0.03230000 0.03180000 0.02780000 0.02120000 0.01360000  
0.00700000 0.00120000 0.00010000

\* CONVOLUTION REQUIRED BETWEEN P.D.F. \*1\* AND P.D.F. \*2\*



# RESULT OF THE CONVOLUTION +

## RESULTING P.C.F.

|             |             |             |             |             |             |             |             |             |             |
|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| 0.00000000  | 0.00000001  | 0.00000007  | 0.00000030  | 0.00000095  | 0.00000274  | 0.00000686  | 0.00001565  | 0.00003283  | 0.00006395  |
| 0.00011658  | 0.00019878  | 0.00031942  | 0.00048925  | 0.00072704  | 0.00105598  | 0.00150820  | 0.00211584  | 0.00290597  | 0.00390952  |
| 0.000516182 | 0.000670803 | 0.000858075 | 0.001079121 | 0.001332798 | 0.001615417 | 0.001919380 | 0.00224222  | 0.002576955 | 0.002922742 |
| 0.00270025  | 0.003610099 | 0.003933693 | 0.004232909 | 0.004500584 | 0.004729242 | 0.004905789 | 0.005015241 | 0.005044075 | 0.004990383 |
| 0.004856523 | 0.004644998 | 0.004367585 | 0.004036290 | 0.003665621 | 0.003270971 | 0.002866558 | 0.002464697 | 0.002074715 | 0.001704786 |
| 0.001362664 | 0.001056740 | 0.000790141 | 0.000564355 | 0.000380403 | 0.000237487 | 0.000134515 | 0.000067510 | 0.000028981 | 0.000010164 |
| 0.00002838  | 0.00000614  | 0.00000107  | 0.00000013  | 0.00000001  | 0.00000000  |             |             |             |             |

## RESULTING DISTRIBUTION FUNCTION

|            |            |            |            |            |            |            |            |            |            |
|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| 0.00000000 | 0.00000001 | 0.00000008 | 0.00000038 | 0.00000134 | 0.00000408 | 0.00001094 | 0.00002659 | 0.00005942 | 0.00012337 |
| 0.00023988 | 0.00043866 | 0.00075808 | 0.00124733 | 0.00197438 | 0.00303036 | 0.00453856 | 0.00665440 | 0.00956037 | 0.01346989 |
| 0.01863172 | 0.02533974 | 0.03392049 | 0.04471170 | 0.05803968 | 0.07419385 | 0.09338765 | 0.11578967 | 0.14155922 | 0.17078663 |
| 0.20348688 | 0.22958787 | 0.27892480 | 0.32125389 | 0.36625973 | 0.41355215 | 0.46261004 | 0.51276246 | 0.56321320 | 0.61310703 |
| 0.66167226 | 0.70812224 | 0.75179809 | 0.79216099 | 0.82881719 | 0.86152691 | 0.89019248 | 0.91463945 | 0.93558660 | 0.95263446 |
| 0.96626110 | 0.97682850 | 0.98472991 | 0.99037347 | 0.99417750 | 0.99655237 | 0.99789752 | 0.99857262 | 0.99886243 | 0.99896407 |
| 0.99899245 | 0.99899859 | 0.99899966 | 0.99899979 | 0.99899980 | 0.99899980 |            |            |            |            |

## RELEVANT DATA

66 NUMBER OF THE HISTOGRAM PCINTS  
 9137.85 ABSCISSA OF THE FIRST POINT  
 10985.11 MEAN VALUE OF THE DISTRIBUTION  
 389.107 STANDARD DEVIATION OF THE MEAN

# RESULT OF THE CONVLUTION +

## CONFIDENCE INTERVALS

|   | P(X) | X-MEAN  | X        |
|---|------|---------|----------|
| 1 | 2.5  | -799.79 | 10185.32 |
| 2 | 5.0  | -677.42 | 10307.69 |
| 3 | 10.0 | -632.50 | 10452.61 |
| 4 | 20.0 | -352.59 | 10632.52 |
| 5 | 40.0 | 313.43  | 11298.54 |
| 6 | 60.0 | 472.64  | 11457.75 |
| 7 | 80.0 | 555.01  | 11580.12 |
| 8 | 97.5 | 694.09  | 11679.20 |



[illegible]



|          |        |       |
|----------|--------|-------|
| 12037.85 | 0.9989 | ***** |
| 12087.85 | 0.9990 | ***** |
| 12137.85 | 0.9990 | ***** |
| 12187.85 | 0.9990 | ***** |
| 12237.85 | 0.9990 | ***** |
| 12287.85 | 0.9990 | ***** |
| 12337.85 | 0.9990 | ***** |
| 12387.85 | 0.9990 | ***** |

RELEVANT DATA OF THE P.D.F. \*1\*

66 NUMBER OF THE HISTOGRAM POINTS  
 9137.85 ABSCISSA OF THE FIRST POINT  
 10985.11 MEAN VALUE OF THE DISTRIBUTION  
 389.107 STANDARD DEVIATION OF THE MEAN

|            |            |            |            |            |            |            |            |            |            |
|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| 0.00000000 | 0.00000001 | 0.00000007 | 0.00000030 | 0.00000095 | 0.00000274 | 0.00000686 | 0.00001565 | 0.00003283 | 0.00006395 |
| 0.00011650 | 0.00019878 | 0.00031942 | 0.00048925 | 0.00072704 | 0.00115598 | 0.00150820 | 0.00211584 | 0.00290597 | 0.00390952 |
| 0.00516182 | 0.00670603 | 0.00858075 | 0.01075121 | 0.01332798 | 0.01615417 | 0.01919380 | 0.02240202 | 0.02576555 | 0.02922142 |
| 0.03270025 | 0.03610059 | 0.03933693 | 0.04232909 | 0.04500584 | 0.04729242 | 0.04905789 | 0.05015241 | 0.05044075 | 0.04990383 |
| 0.04856523 | 0.04644998 | 0.04367585 | 0.04036290 | 0.03665621 | 0.03270971 | 0.02866558 | 0.02464697 | 0.02074715 | 0.01704786 |
| 0.01362664 | 0.01056740 | 0.00790141 | 0.00564355 | 0.00380403 | 0.00237487 | 0.00134515 | 0.00067510 | 0.00028981 | 0.00010164 |
| 0.00002838 | 0.00000614 | 0.00000107 | 0.00000013 | 0.00000001 | 0.00000000 |            |            |            |            |

RELEVANT DATA OF THE P.D.F. \*2\*

18 NUMBER OF THE HISTOGRAM POINTS  
 10315.00 ABSCISSA OF THE FIRST POINT  
 11190.00 MEAN VALUE OF THE DISTRIBUTION  
 141.000 STANDARD DEVIATION OF THE MEAN

|            |            |            |            |            |            |            |            |            |            |
|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| 0.00227790 | 0.00424953 | 0.01015516 | 0.02142759 | 0.03992106 | 0.06567166 | 0.09539098 | 0.12234697 | 0.13855934 | 0.13855894 |
| 0.12234697 | 0.09539098 | 0.06567166 | 0.03992106 | 0.02142759 | 0.01015516 | 0.00424953 | 0.00227790 |            |            |

2-1. CONVOLUTION REQUIRED BETWEEN P.D.F. \*1\* AND P.D.F. \*2\*

# RESULT OF THE CONVOLUTION 2-1

## RESULTING P<sub>0</sub>D<sub>0</sub>F<sub>0</sub>

|            |            |            |            |            |            |            |            |            |            |
|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |

## RESULTING DISTRIBUTION FUNCTION

|            |            |            |            |            |            |            |            |            |            |
|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |
| 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 | 0.00000000 |

## RELEVANT DATA

83 NUMBER OF THE HISTOGRAM POINTS  
 -2027.15 ABSCISSA OF THE FIRST POINT  
 -203.18 MEAN VALUE OF THE DISTRIBUTION  
 413.879 STANDARD DEVIATION OF THE MEAN

# RESULT OF THE CONVOLUTION 2-1

## CONFIDENCE INTERVALS

|   | P(X) | X-MEAN  | X       |
|---|------|---------|---------|
| 1 | 2.5  | -790.01 | -993.19 |
| 2 | 5.0  | -680.45 | -883.64 |
| 3 | 10.0 | -548.01 | -751.19 |
| 4 | 20.0 | -277.48 | -580.67 |
| 5 | 40.0 | 227.46  | 124.27  |
| 6 | 60.0 | 518.07  | 314.88  |
| 7 | 80.0 | 672.59  | 470.40  |
| 8 | 97.5 | 809.52  | 606.34  |



```

MASS PDF
-2027.15 0.00000
-1977.15 0.00000
-1927.15 0.00000
-1877.15 0.00000
-1827.15 0.00000
-1777.15 0.00000
-1727.15 0.00000
-1677.15 0.00000
-1627.15 0.00000
-1577.15 0.00000
-1527.15 0.00000
-1477.15 0.00001
-1427.15 0.00001
-1377.15 0.00003
-1327.15 0.00005
-1277.15 0.00009
-1227.15 0.00014
-1177.15 0.00022
-1127.15 0.00032
-1077.15 0.00045
-1027.15 0.00062
-977.15 0.00083
-927.15 0.00107
-877.15 0.00134
-827.15 0.00165
-777.15 0.00197
-727.15 0.00232
-677.15 0.00268
-627.15 0.00304
-577.15 0.00340
-527.15 0.00373
-477.15 0.00403
-427.15 0.00429
-377.15 0.00450
-327.15 0.00465
-277.15 0.00473
-227.15 0.00475
-177.15 0.00470
-127.15 0.00459
-77.15 0.00443
-27.15 0.00422
22.85 0.00397
72.85 0.00369
122.85 0.00339
172.85 0.00308
222.85 0.00276
272.85 0.00245
322.85 0.00214
372.85 0.00184
422.85 0.00157
472.85 0.00131
522.85 0.00108
572.85 0.00088
622.85 0.00070
672.85 0.00056
722.85 0.00043
772.85 0.00033
822.85 0.00025

```

|         |        |   |
|---------|--------|---|
| 872.85  | 0.0018 | * |
| 922.85  | 0.0013 | * |
| 972.85  | 0.0009 | * |
| 1022.85 | 0.0007 |   |
| 1072.85 | 0.0005 |   |
| 1122.85 | 0.0003 |   |
| 1172.85 | 0.0002 |   |
| 1222.85 | 0.0001 |   |
| 1272.85 | 0.0001 |   |
| 1322.85 | 0.0000 |   |
| 1372.85 | 0.0000 |   |
| 1422.85 | 0.0000 |   |
| 1472.85 | 0.0000 |   |
| 1522.85 | 0.0000 |   |
| 1572.85 | 0.0000 |   |
| 1622.85 | 0.0000 |   |
| 1672.85 | 0.0000 |   |
| 1722.85 | 0.0000 |   |
| 1772.85 | 0.0000 |   |
| 1822.85 | 0.0000 |   |
| 1872.85 | 0.0000 |   |
| 1922.85 | 0.0000 |   |
| 1972.85 | 0.0000 |   |
| 2022.85 | 0.0000 |   |
| 2072.85 | 0.0000 |   |

MASS CISTR.

-2027.15 0.0000  
-1977.15 0.0000  
-1927.15 0.0000  
-1877.15 0.0000  
-1827.15 0.0000  
-1777.15 0.0000  
-1727.15 0.0000  
-1677.15 0.0000  
-1627.15 0.0000  
-1577.15 0.0000  
-1527.15 0.0001  
-1477.15 0.0001  
-1427.15 0.0003  
-1377.15 0.0005  
-1327.15 0.0010  
-1277.15 0.0019  
-1227.15 0.0033  
-1177.15 0.0054  
-1127.15 0.0086  
-1077.15 0.0132  
-1027.15 0.0194  
-977.15 0.0277  
-927.15 0.0383  
-877.15 0.0517  
-827.15 0.0682  
-777.15 0.0879  
-727.15 0.1112  
-677.15 0.1380  
-627.15 0.1684  
-577.15 0.2024  
-527.15 0.2397  
-477.15 0.2800  
-427.15 0.3229  
-377.15 0.3678  
-327.15 0.4143  
-277.15 0.4616  
-227.15 0.5091  
-177.15 0.5561  
-127.15 0.6020  
-77.15 0.6463  
-27.15 0.6885  
22.85 0.7283  
72.85 0.7652  
122.85 0.7991  
172.85 0.8299  
222.85 0.8576  
272.85 0.8820  
322.85 0.9034  
372.85 0.9218  
422.85 0.9375  
472.85 0.9506  
522.85 0.9615  
572.85 0.9703  
622.85 0.9773  
672.85 0.9829  
722.85 0.9872  
772.85 0.9905  
822.85 0.9930

[illegible]

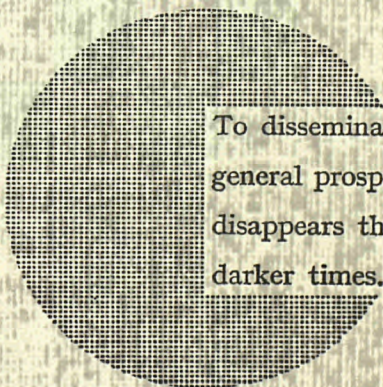
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Alfred Nobel



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